

# Tunnel Diode Loaded Rectangular Microstrip Antenna with Passive Components for Millimeter Range

Priti Sharma, Tazeem Ahmad Khan, B. R. Vishwakarma

**Abstract:-** The present work describes the circuit model based analysis of tunnel diode (Active Device) loaded microstrip antenna with parasitic elements using equivalent circuit concept. To optimize the antenna characteristics a study has been carried out as a function of tunnel diode space with microstrip patch. It is observed that the antenna can be operated over a range of frequency from 39.163GHz to 57.688GHz for Germanium tunnel diode loaded patch just by varying the value of passive elements. The return loss improves to -43.3dB.

**Keywords:** Microstrip Antenna; Active tunnel diode loaded patch and passive elements patch,

## I. INTRODUCTION

In high-performance aircraft, spacecraft, satellite, and missile applications, where size, weight, cost, performance, ease of installation, and aerodynamic profile are constraints, low-profile antennas may be required. Microstrip antenna have attracted widespread interest due to their small size, light weight, low cost, low profile. Presently there are many other government and commercial applications, conformable to planar and nonplanar surfaces, inexpensive to manufacture using modern printed-circuit technology but their low gain and narrow bandwidth and low power capacity make limited use of these antenna. In this paper here proposed a tunnel diode-loaded rectangular patch for achieving the frequency tenability in the millimeter range. The equivalent circuit of a tunnel diode consists of a junction capacitance  $C_d$ , which varies with the bias voltage which in turn changes the operating frequency. The major advantage of using a tunnel diode is its low voltage and power requirements, vary wide temperature range of operation and extremely high speed of operation. Various antenna parameters such as input impedance, VSWR, Return loss, frequency range etc are obtained by selecting passive element value.

## II. ANTENNA DESIGN

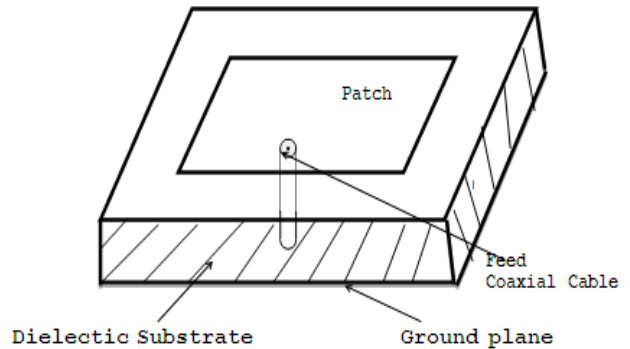
Tunnel diode loaded microstrip antenna is shown in figure 1. A microstrip device in its simplest form consists of sandwich of two parallel conducting layers separated by a single thin substrate [4]. The lower conductor function as a ground plane and the upper conductor may be a simple resonant rectangular or circular patch, a resonant dipole, or a monolithically printed array of patches or dipoles and the associated feed network.

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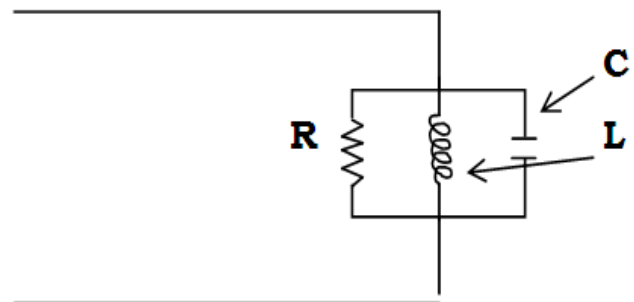
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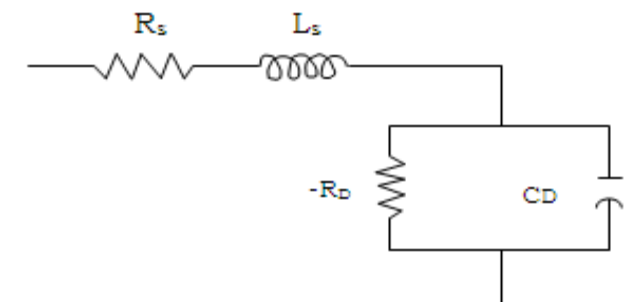
**Figure 1 Tunnel Diode Loaded Rectangular Microstrip Antenna**

The equivalent circuit of a rectangular patch microstrip antenna is a parallel combination of resistance  $R$ , inductance  $L$ , and capacitance  $C$  as shown in fig 2.



**Figure 2 Equivalent Circuit of Rectangular Micro Strip Patch**

The equivalent circuit [1], [2] for a tunnel diode has a resistance  $R_s$  and inductance  $L_s$  in series and the negative resistance and junction capacitance  $C_d$  in parallel as shown in fig. 3.



**Figure 3 Equivalent Circuit of Tunnel Diode**

## Tunnel Diode Loaded Rectangular Microstrip Antenna with Passive Components for Millimeter Range

Inductor  $L_s$  and resistor  $R_s$  represent parasitic element Capacitor  $C_d$  capacitance caused mainly by the internal depletion region. Resistor  $R_d$  represents the ac negative resistance of the device. The tunnel diode equivalent circuit acts like a series resonant circuit where its input terminals are ac short circuited. The value of resistance  $R$ , inductance  $L$ , and capacitance  $C$  are giving as

$$C = \frac{1}{2} C_{dc} \cos^{-2}(\pi y_0/l)$$

With  $C_{dc}$  being the dc patch capacitance[6]

$$C_{dc} = \frac{\epsilon l W}{h}$$

so

$$C = \frac{1}{2} \frac{\epsilon W l}{h} \cos^{-2}(\pi y_0/l)$$

$$\epsilon_e = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left(1 + \frac{10h}{W}\right)^{-1/2}$$

Where  $\epsilon_r$  is the relative permittivity of the substrate material.

Where  $y_0$  = Y-coordinate of feed point

$h$  = Thickness of the substrate

$\epsilon_0$  = Permittivity of free space

$\epsilon_e$  = Effective dielectric constant

$l$  = Length of the patch.

$W$  = Width of the patch.

$c$  = Velocity of light

In the millimeter wave range, the calculations for length and width, are done according to the moment method solution of a printed rectangular radiating element on a grounded dielectric slab[3]. Width ( $W$ ) is  $0.3 \lambda_0$ , where  $\lambda_0$  is the free space wavelength. The patch ( $\epsilon_r$ ) stops resonating at  $h > 0.11 \lambda_0$ . Hence, we have taken  $h = 0.1 \lambda_0$  and correspondingly  $l = 0.25 / \lambda_0$ .

$$L = \frac{1}{\omega^2 C}$$

$$R = \frac{Q_r}{\omega C}$$

The combined equivalent circuit of the tunnel diode and the microstrip patch is shown in fig.4. When a bias voltage  $V$  is applied to the terminals, it is transferred to the external circuit because of the negative resistance of the tunnel diode

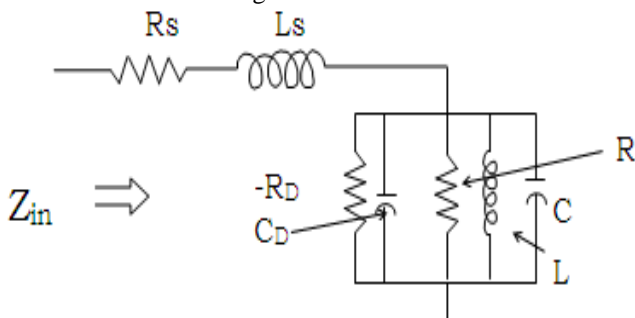


Figure 4 Combined Equivalent Circuit of Rectangular Patch Antenna with Tunnel Diode

**2.1. Impedance :** The input impedance is calculated as

$$Z_{in} = (R_s + j\omega L_s) + \frac{j\omega L R R_d}{j\omega L(R_d - R) - \omega^2 L R R_d(C + C_d) + R R_d}$$

**2.2. Operating frequency :** The operating frequency of a tunnel diode oscillator circuit is given by [4]

$$f_0 = \frac{1}{2\pi} \frac{\sqrt{[(C + C_d)(2R R_d L^2 + 2R^2 L L_d + R^2 L^2) + L^2 L_d] \pm [(C + C_d)(2R^2 L L_d + 2R^2 R L^2 + R^2 L^2) + L^2 L_d]}}{2\pi R^2 L L_d (C + C_d)}$$

**2.3 Design specifications** for microstrip patch antenna

The detail designed frequency of the rectangular patch antenna is given in Table 1.[7]

Components	Values
Series resistance ( $R_s$ )	4.5 $\Omega$
Series inductance ( $L_s$ )	0.169 nH
Negative resistance ( $R_d$ )	-106 $\Omega$
Junction capacitance ( $C_d$ )	0.03550 pF
Charge concentration ( $np/(n+p)$ )	$2.295 * 10^{17} \text{ cm}^{-3}$
Junction area ( $A$ )	$4.906 * 10^{-10} \text{ cm}^2$
Diffusion potential ( $V_d$ )	1.1 V
Design frequency	(f) 50 GHz
Element width ( $W$ )	1.8 mm
Element length ( $l$ )	1.60 mm
Resistance ( $R$ )	130 $\Omega$
Inductance ( $L$ )	0.12843 nH
Capacitance ( $C$ )	0.0800 pF

## III. RESULT AND DISCUSSION

The range of frequency obtainable for operation is '18525MHz'. And the antenna could be operated in the millimeter wave range (39.163GHz - 57.688GHz). Variation of the magnitude of input impedance ( $Z_{in}$ ) with frequency is shown in figure (5). Maximum value of  $Z_{in}$  is 62.86  $\Omega$ . Variation of the VSWR with frequency is shown in figure (6). The VSWR should be less than 2. VSWR is 1.259. The figure (7), shows the variation of return loss with frequency. The return loss should be less than -10dB. It is -43.3dB.

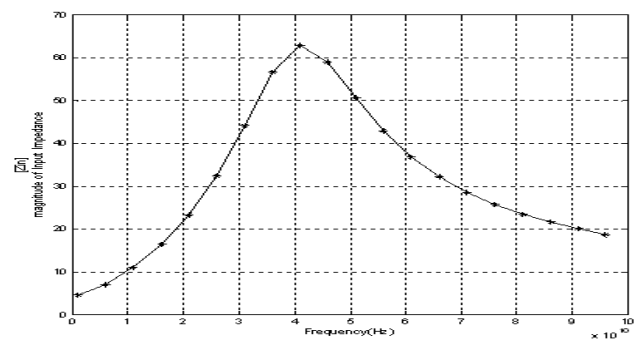


Figure 5: Variation of Magnitude of Input Impedance with Frequency for Ge Tunnel Diode Loaded Patch

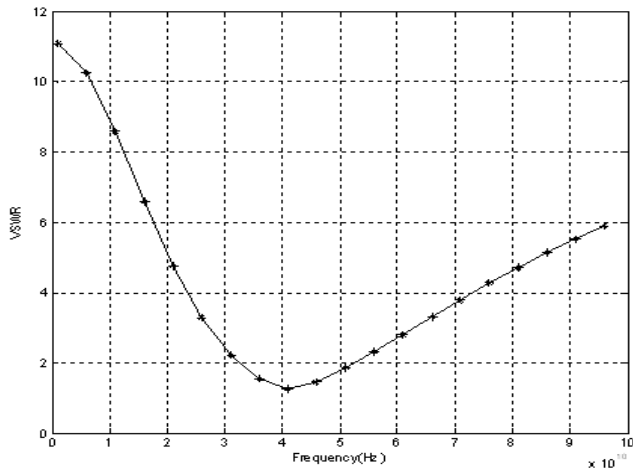


Figure 6 Variation of VSWR with Frequency for Ge Tunnel Diode Loaded Patch

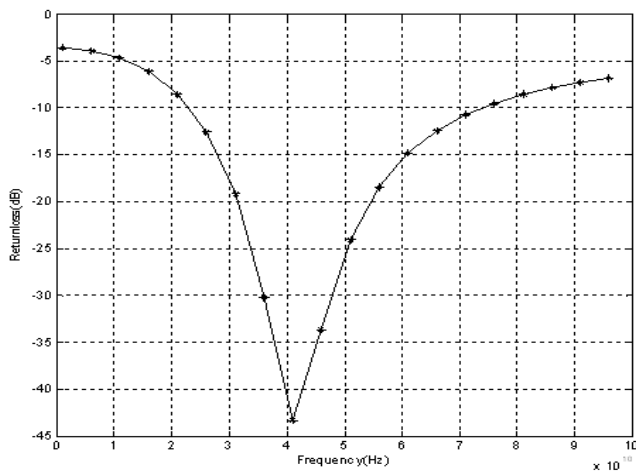


Figure 7 Variation of Return Loss with Frequency for Ge Tunnel Diode Loaded Patch

#### IV. CONCLUSION

In this paper investigate Performance of equivalent Circuit of Tunnel Diode Loaded Rectangular Microstrip Antenna at 41GHz Frequency Using Different value of Passive components. It concluded that the varying the value of passive element (R L & C) performance enhances the VSWR and Return loss of tunnel diode loaded Microstrip patch antenna. It is concluded from the above analysis that the bandwidth, return loss of the tunnel diode loaded Microstrip patch antenna is improved. In this way the performance of its can be improve by varying the value of passive elements. In future, we can performance enhancement using other material in place of Ge.

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