

Optimum Heat Shielding Effect of an Engine by using Aluminium, Zirconium Materials

Kunchala Krishna, H Ameresh, O Rajender

Abstract: A warmth shield is intended to shield a substance from retaining extreme warmth from an outside source by either dispersing, reflecting or basically engrossing the warmth. Because of the a lot of warmth radiated by inward burning motors, heat shields are utilized on most motors to shield segments and bodywork from warmth.

Just as assurance, compelling warmth shields can give a presentation advantage by lessening the under-cap temperatures, accordingly decreasing the admission temperature. Warmth protecting is important to avert motor warmth from harming heat-delicate parts. Most of more established vehicles utilize straightforward steel warmth protecting to diminish warm radiation and convection.

It is currently most regular for present day vehicles are to utilize aluminum warmth protecting which has a lower thickness, can be effectively shaped and does not erode similarly as steel. Higher execution vehicles are starting to utilize fired warmth protecting as this can withstand far higher temperatures just as further decreases in warmth move.

Keywords : — Heat shielding system design, Temperature, Thermal analysis, aluminum alloy, , MgO–ZrO₂ materials, Ansys.

I. INTRODUCTION

Heat shield In this investigation, right off the bat, warm examination done on motor ensure Heat protecting framework, made of aluminum composite and MgO–ZrO₂ material. the consequences of Heat protecting frameworks materials are contrasted and one another. The impacts of materials on the warm practices of the Heat protecting frameworks are finished. It has been shown that the maximum and min temperature of the Heat shielding systems . Temperatures, radiation, convection, Thermal analysis done by the Ansys software. Model Design was done by the CATIA software. The adaptable warmth shield is typically produced using flimsy aluminum sheeting, sold either level or in a roll, and is twisted by hand, by the fitter. Elite adaptable warmth shields now and then incorporate additional items, for example, clay protection connected through plasma splashing. These most recent items are typical in top-end motorsports, for example, Formula - 1 vehicle.

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II. MATERIAL SELECTION

Material selection The physical properties of aluminum alloys, zirconium, steel alloys - reflectivity and emissivity, warm conductivity and particular hotness limit - make it to the perfect material for the manufacture of high-temperature shields.

The high reflectivity and low emissivity of the aluminum alloy, zirconium surface (actually when secured with the regular aluminum oxide film) guarantee that aluminum alloy and zirconium, assimilates and re-discharges minimal infrared radiation.

The high warm conductivity of aluminum alloy, zirconium, guarantees that hotness is immediately directed far from potential problem areas in the hotness shield. This material has added a high specific hotness limit. This infers the temperature increase in the wake of holding a given proportion of hotness essentialness is lower than for some various materials.

Aluminum combination, zirconium, sheets, and thwarts are fitting to satisfy the diverse amassing and organization necessities of auto high-temperature shields. A most basic need is a fair formability remembering the true objective to meet the stunning pack imprisonments. Hotness shields need to cover the hot fragment the degree this would be conceivable and as close as could be permitted.

III. DESIGN

- A high-temperature shield is intended to shield some pieces of supplies from retaining unnecessary hotness from an outside source by scattering, reflecting or just engrossing the hotness.
- Hotness shields are intended to shield a segment from engrossing inordinate high temperature either by dispersing, reflecting or retaining the high temperature. In an auto fueled by an inward burning motor, the fumes framework from the motor ventilation system to the tailpipe is the greatest maker of hotness after the motor itself.
- The surfaces of the parts that convey the fumes gasses can achieve temperatures up to around 900°C. Since depletes regularly pass close essential (and thermally touchy) segments, it is particularly critical to shield the delicate parts and modules from hotness douse, additionally to forestall nearby overheating of the auto body.

A. Design Specifications

The width of the heat shelled is 100,143mm

Curvatures Radius 180, 45 and 7mm

The Bounding box

X-axis 85mm,

Y-axis 159.5mm

Z-axis 115.26mm

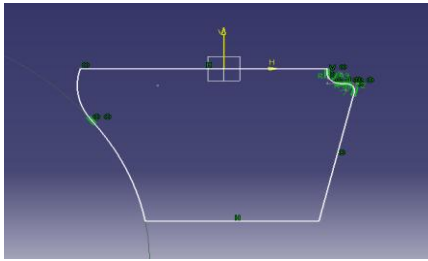
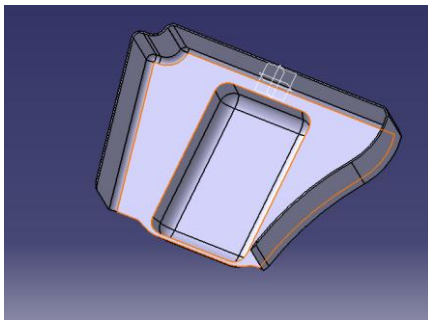
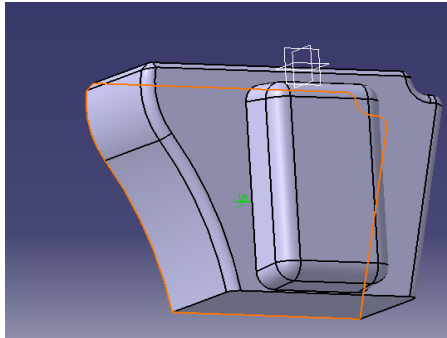


Fig 2.1 Design of heat shield



2.2 Model heat shield

B. Transient Thermal analysis

You can use steady-state thermal analysis to determine temperatures, thermal gradients, heat flow rates, and heat fluxes in an object that are caused by thermal loads that do not vary over time. Such loads include the following:

- Convections
- Radiation
- Heat flow rates
- Heat fluxes (heat flow per unit area)
- Heat generation rates (heat flow per unit volume)
- Constant temperature boundaries

IV. RESULTS AND DISCUSSION

Aluminum alloy properties

constants

Density	$2.77 \times 10^{-6} \text{ kg mm}^3$
Coefficient of Thermal Expansion	$2.3 \times 10^{-5} \text{ }^\circ\text{C}^{-1}$
Specific Heat	$8.75 \times 10^5 \text{ MJ kg}^2$

B.CONTOURS OF ALUMINIUM

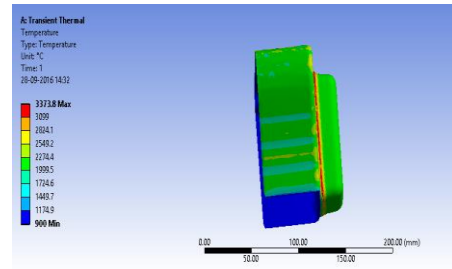


Fig 3.1 Contour of Temperature

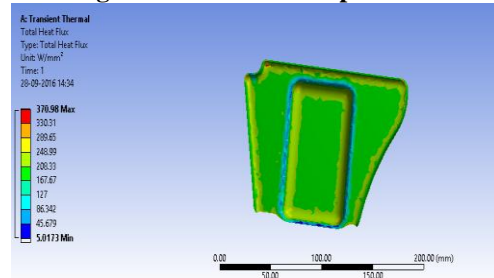


Fig 3.2 Contour of Total heat flux

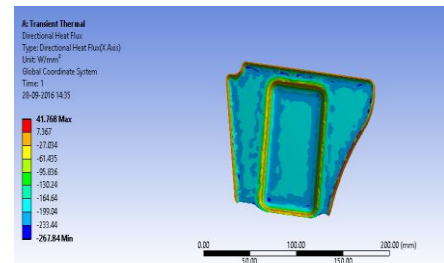


Fig 3.3 Contour Directional heat flux

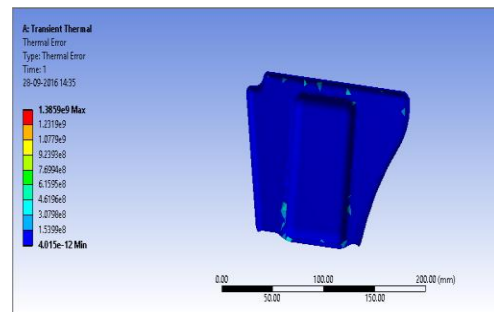


Fig 3.4 Contour of thermal error

C.Results for Aluminium

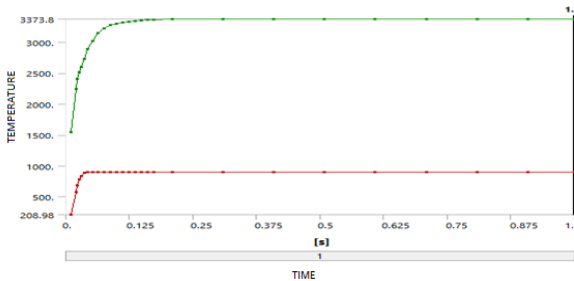
Variation of Temperature

Time [s]	Minimum	Maximum
$1. \times 10^{-2}$	1327.6	1.0851×10^9
2×10^{-2}	2345.3	1.0498×10^9
2.3333×10^{-2}	1673.8	1.2701×10^9
2.6667×10^{-2}	476.96	1.3806×10^9
3.089×10^{-2}	229.28	1.4386×10^9
3.6202×10^{-2}	88.117	1.4596×10^9
4.3284×10^{-2}	11.17	1.4576×10^9
5.255×10^{-2}	2.9699	1.4437×10^9
6.3467×10^{-2}	0.33242	1.4278×10^9
7.5145×10^{-2}	5.3473×10^{-2}	1.4148×10^9



8.7102 x10 ⁻²	3.6627 x10 ⁻³	1.4055 x 10 ⁹
9.9161 x10 ⁻²	4.9146 x10 ⁻⁴	1.3991 x 10 ⁹
0.11127	5.1465 x10 ⁻⁵	1.3947 x 10 ⁹
0.1234	5.011 x10 ⁻⁶	1.3918 x 10 ⁹
0.13555	5.1675 x10 ⁻⁷	1.3899 x 10 ⁹
0.14771	4.2827 x10 ⁻⁸	1.3886 x 10 ⁹
0.15989	2.0591 x10 ⁻⁹	1.3877 x 10 ⁹
0.17207	1.4025 x10 ⁻¹⁰	1.3871 x 10 ⁹
0.20862	8.6094 x10 ⁻¹¹	1.3864 x 10 ⁹
0.30862	4.1414 x10 ⁻¹²	1.386 x 10 ⁹
0.40862	4.0213 x10 ⁻¹³	1.3859 x 10 ⁹
0.50862	4.0153 x10 ⁻¹⁴	
0.60862	4.015 x10 ⁻¹⁵	
0.70862		
0.80862		
0.90862		
1		

(Aluminium) Temperature V/s Time



The Aluminum Minimum temperature has 208.98 at Time 1x10⁻² sec gradually increases 900°C Maximum temperature 1541.9 at Time 1x10⁻² sec is gradually increased 3364.4 at Time 1 sec.

Time [s]	Minimum [°C]	Maximum [°C]
1x10-2	208.98	1541.9
2x10 ⁻²	577.22	2247.4
2.3333x10 ⁻²	687.79	2407
2.6667x10 ⁻²	776.67	2513.7
3.09E-02	829.79	2596.3
3.6202x10 ⁻²	887.36	2730.2
4.3284x10 ⁻²	900	2887.2
5.255x10 ⁻²		3021.5
6.3467x10 ⁻²		3143.7
7.5145x10 ⁻²		3223.4
8.7102x10 ⁻²		3272.7
9.9161x10 ⁻²		3302.5
0.11127		3320.6
0.1234		3331.4
0.13555		3340.7
0.14771		3352
0.15989		3359.5
0.17207		3364.4

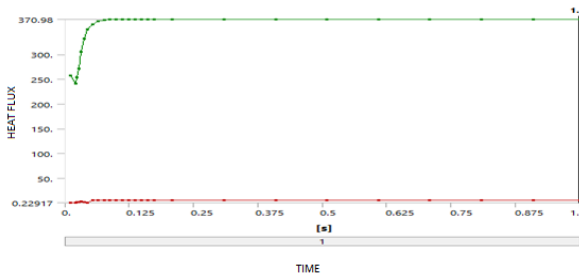
0.20862		3370.1
0.30862		3373.1
0.40862		3373.7
0.50862		3373.8
0.60862		
0.70862		
0.80862		
0.90862		

Variation of Total Heat Flux

Time [s]	Minimum [W/mm ²]	Maximum [W/mm ²]
1 x10 ⁻²	0.43948	257.75
2 x10 ⁻²	0.22917	240.55
2.3333x10 ⁻²	0.93095	253.52
2.6667x10 ⁻²	1.1071	270.75
3.089x10 ⁻²	2.7545	305.4
3.6202x10 ⁻²	2.0941	331.7
4.3284x10 ⁻²	0.56569	350.29
5.255x10 ⁻²	5.0437	361.5
6.35E-02	5.3828	367.03
7.51E-02	5.1348	369.4
8.7102x10 ⁻²	5.0545	370.36
9.9161x10 ⁻²	5.029	370.74
0.11127	5.021	370.88
0.1234	5.0185	370.94
0.13555	5.0177	370.96
0.14771	5.0174	370.97
0.15989		
0.17207	5.0173	370.98
0.20862		
0.30862		
0.40862		
0.50862		
0.60862		
0.70862		
0.80862		
0.90862		
1		

The Aluminium Minimum Total heat flux has 0.43948 [W/mm²] at Time 1x10⁻² sec gradually increases 5.0173 at time 1sec Maximum Total heat flux 257.75 at Time 1x10² sec is gradual increases 370.98 [W/mm²] at Time 1 sec.

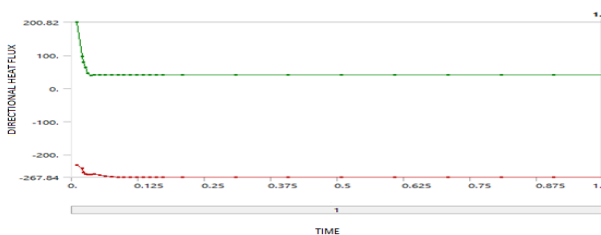
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(Aluminium) Heat Flux V/s Time
Variation of Directional Heat Flux

Time [s]	Minimum [W/mm ²]	Maximum [W/mm ²]
1. x10 ⁻²	-230.62	200.82
2 x10 ⁻²	-240.53	97.07
2.3333x10 ⁻²	-253.5	79.671
2.6667x10 ⁻²	-258.28	63.657
3.089x10 ⁻²	-259.78	45.521
3.6202x10 ⁻²	-259.36	40.218
4.3284x10 ⁻²	-257.78	41.089
5.255x10 ⁻²	-260.89	41.512
6.3467x10 ⁻²	-264.91	41.68
7.5145x10 ⁻²	-266.67	41.739
8.7102x10 ⁻²	-267.38	41.759
9.9161x10 ⁻²	-267.66	41.765
0.11127	-267.77	41.767
0.1234	-267.82	41.768
0.13555	-267.83	
0.14771	-267.84	
0.15989		
0.17207		
0.20862		
0.30862		
0.40862		
0.50862		
0.60862		
0.70862		
0.80862		
0.90862		
1		

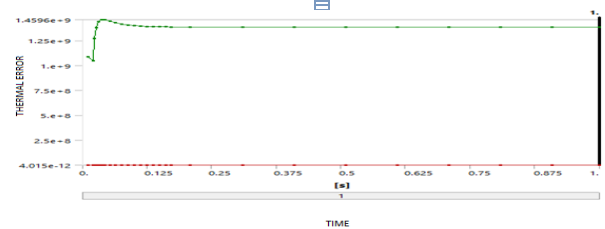
The Aluminium Minimum Directional heat flux has -230.62 [W/mm²] at Time 1x10⁻² sec gradually increases -267.84 at 1 sec Maximum Directional heat flux 200.82 at Time 1x10⁻² sec is gradually increased 35.995 [W/mm²] at Time 1 sec



(Aluminium) Directional Heat Flux V/s Time
Variation of Thermal Error

Time [s]	Minimum	Maximum
1. x10 ⁻²	1327.6	1.0851 x 10 ⁹
2 x10 ⁻²	2345.3	1.0498 x 10 ⁹
2.3333 x10 ⁻²	1673.8	1.2701 x 10 ⁹
2.6667 x10 ⁻²	476.96	1.3806 x 10 ⁹
3.089 x10 ⁻²	229.28	1.4386 x 10 ⁹
3.6202 x10 ⁻²	88.117	1.4596 x 10 ⁹
4.3284 x10 ⁻²	11.17	1.4576 x 10 ⁹
5.255 x10 ⁻²	2.9699	1.4437 x 10 ⁹
6.3467 x10 ⁻²	0.33242	1.4278 x 10 ⁹
7.5145 x10 ⁻²	5.3473 x10 ⁻²	1.4148 x 10 ⁹
8.7102 x10 ⁻²	3.6627 x10 ⁻³	1.4055 x 10 ⁹
9.9161 x10 ⁻²	4.9146 x10 ⁻⁴	1.3991 x 10 ⁹
0.11127	5.1465 x10 ⁻⁵	1.3947 x 10 ⁹
0.1234	5.011 x10 ⁻⁶	1.3918 x 10 ⁹
0.13555	5.1675 x10 ⁻⁷	1.3899 x 10 ⁹
0.14771	4.2827 x10 ⁻⁸	1.3886 x 10 ⁹
0.15989	2.0591 x10 ⁻⁹	1.3877 x 10 ⁹
0.17207	1.4025 x10 ⁻¹⁰	1.3871 x 10 ⁹
0.20862	8.6094 x10 ⁻¹¹	1.3864 x 10 ⁹
0.30862	4.1414 x10 ⁻¹²	1.386 x 10 ⁹
0.40862	4.0213 x10 ⁻¹³	1.3859 x 10 ⁹
0.50862	4.0153 x10 ⁻¹⁴	
0.60862	4.015 x10 ⁻¹⁵	
0.70862		
0.80862		
0.90862		
1		

The Aluminium Minimum Thermal error 1327.6 has at Time 1x10⁻² gradually increases 4.015x 10⁻¹⁵ sec Maximum Thermal error 1.0851 x 10⁹ at Time 1x10⁻² sec increases 1.3859x10⁹ at Time 1 sec.



(Aluminium) Thermal Error V/s Time

Zirconium properties

Constants

Density	5.7x10 ⁻⁶ kg mmx10 ⁻³
Thermal Conductivity	3x10 ⁻³ W/mm ² x10 ⁻²
Specific Heat	9x10 ⁻⁵ mJ kgx10 ⁻²

Isotropic Elasticity

Temperature C	Young's Modulus MPa	Poisson's Ratio	Bulk Modulus MPa	Shear Modulus MPa
900	1.8x10 ⁵	0.3	1.5x10 ⁵	69231

E Contours of Zirconium

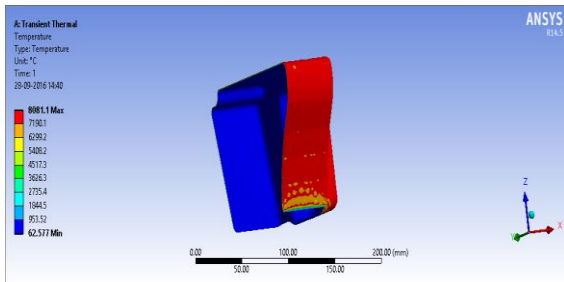


Fig 3.5 Contour of Temperature

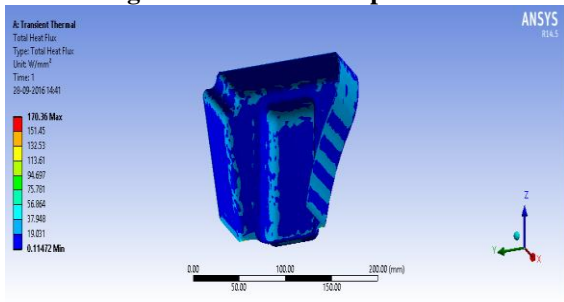


Fig3.6 Contour of Total Heat Flux

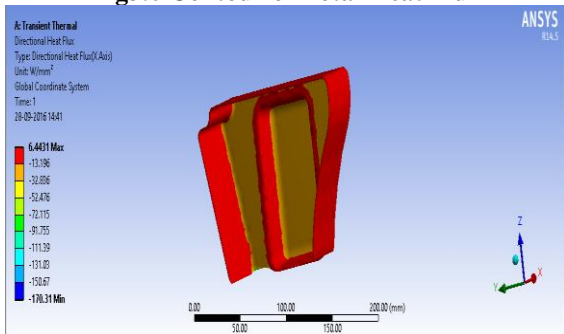


Fig3.7 Contour of Directional Heat Flux

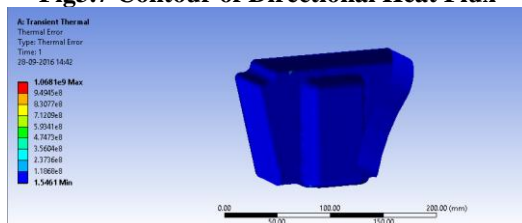
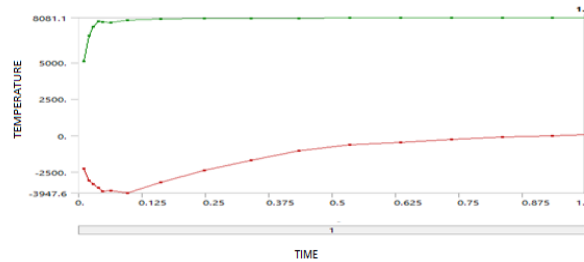


Fig3.8 Contour of Thermal Error

0.73528	-278.53	8077
0.83528	-93.295	8079.1
0.93528	0.35442	8080.5
1	62.577	8081.1



(zirconium) Temperature V/s Time

The above figure 5.22 gives the relation between Temperature and Time. This figure gives the variation of temperature according to the time of the zirconium

The zirconium Minimum temperature has -2256.9 at Time 1×10^{-2} sec gradually increases 62.577 at Time 1sec Maximum temperature 5095 at Time 1×10^{-2} sec is gradual increases 8081.1 at Time 1 sec

Variation of Total Heat Flux

Time [s]	Minimum [°C]	Maximum [°C]
1×10^{-2}	208.98	1541.9
2×10^{-2}	577.22	2247.4
2.3333×10^{-2}	687.79	2407
2.6667×10^{-2}	776.67	2513.7
3.09E-02	829.79	2596.3
3.6202×10^{-2}	887.36	2730.2
4.3284×10^{-2}	900	2887.2
5.255×10^{-2}		3021.5
6.3467×10^{-2}		3143.7
7.5145×10^{-2}		3223.4
8.7102×10^{-2}		3272.7
9.9161×10^{-2}		3302.5
0.11127		3320.6
0.1234		3331.4
0.13555		3340.7
0.14771		3352
0.15989		3359.5
0.17207		3364.4
0.20862		3370.1
0.30862		3373.1
0.40862		3373.7
0.50862		3373.8
0.60862		
0.70862		
0.80862		
0.90862		
1		

F. Results for Zirconium

Variation of Temperature

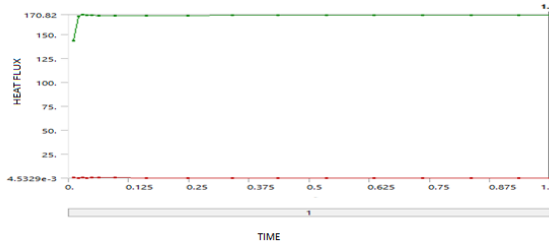
Time [s]	Minimum [°C]	Maximum [°C]
1×10^{-2}	-2256.9	5095
2×10^{-2}	-3068.1	6849
2.927×10^{-2}	-3334.6	7473.2
3.854×10^{-2}	-3573.8	7832.6
4.781×10^{-2}	-3811	7784.2
6.3023×10^{-2}	-3790.9	7753.5
9.5877×10^{-2}	-3947.6	7914.9
0.161	-3226.3	7978.8
0.24734	-2390.5	8020.1
0.33956	-1685.5	8043.7
0.43528	-1051.4	8058.8
0.53528	-628.93	8068
0.63528	-457.61	8073.6

The zirconium Minimum Total heat flux has 0.32714 [W/mm²] at Time 1×10^{-2} sec gradually increases 0.11472 at 1sec and Maximum Total heat



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flux 143.45 at Time 1×10^{-2} sec is gradual increases 170.36 [W/mm²]at Time 1 sec.



(zirconium) Heat Flux V/s Time

The above figure 5.23 gives the relation between heat flux and Time. This figure gives the variation of heat flux according to the time of the zirconium

Directional Heat Flux

Time [s]	Minimum [W/mm ²]	Maximum [W/mm ²]
1. $\times 10^{-2}$	-143.38	59.056
2. $\times 10^{-2}$	-168.8	63.486
2.927 $\times 10^{-2}$	-170.76	64.457
3.854 $\times 10^{-2}$	-170.19	61.971
4.781 $\times 10^{-2}$	-169.9	55.96
6.3023 $\times 10^{-2}$	-169.64	49.685
9.5877 $\times 10^{-2}$	-169.54	38.615
0.161	-169.66	26.352
0.24734	-169.88	18.524
0.33956	-170.06	13.887
0.43528	-170.17	11.153
0.53528	-170.24	10.09
0.63528	-170.27	9.0775
0.73528	-170.29	8.3392
0.83528	-170.3	7.6289
0.93528	-170.31	6.9083
1		6.4431

The zirconium Minimum Directional heat flux has -143.38 [W/mm²] at Time 1×10^{-2} sec gradually increases-170.31 at 1sec and Maximum Directional heat flux 59.056 at Time 1×10^{-2} sec is gradual increases 6.4431[W/mm²] at Time 1 sec

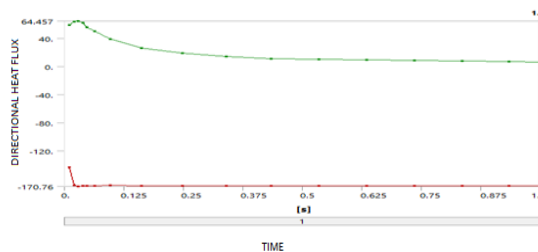


Fig4.7(zirconium) Directional Heat Flux V/s Time

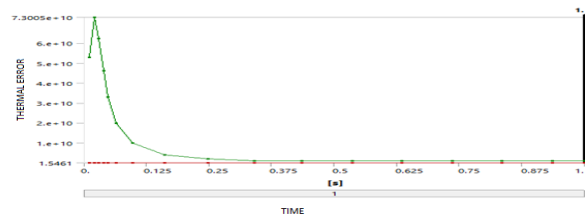
The above figure gives the relation between Directional heat flux and Time. This figure gives the variation of heat flux according to the time of the zirconium

Variation of Thermal Error

Time [s]	Minimum	Maximum
1 $\times 10^{-2}$	93570	5.2896 $\times 10^{10}$
2. $\times 10^{-2}$	2.3545 $\times 10^5$	7.3005 $\times 10^{10}$
2.927 $\times 10^{-2}$	2.574 $\times 10^5$	6.2259 $\times 10^{10}$
3.854 $\times 10^{-2}$	2.6065 $\times 10^5$	4.6183 $\times 10^{10}$
4.781 $\times 10^{-2}$	2.1366 $\times 10^5$	3.2998 $\times 10^{10}$

6.3023 $\times 10^{-2}$	1.7304 $\times 10^5$	1.9787 $\times 10^{10}$
9.5877 $\times 10^{-2}$	93482	1.0001 $\times 10^{10}$
0.161	20195	4.0474 $\times 10^9$
0.24734	4371.1	1.9803 $\times 10^9$
0.33956	1834.3	1.1001 $\times 10^9$
0.43528	686.82	9.4178 $\times 10^8$
0.53528	56.065	1.0036 $\times 10^9$
0.63528	38.284	1.037 $\times 10^9$
0.73528	26.508	1.0545 $\times 10^9$
0.83528	14.187	1.0631 $\times 10^9$
0.93528	3.7868	1.0669 $\times 10^9$
1	1.5461	1.0681 $\times 10^9$

The zirconium Minimum Thermal error has 93570 at Time 1×10^{-2} sec gradually increases 1.5461 at 1sec Maximum Thermal error 5.2896 $\times 10^{10}$ at Time 1×10^{-2} sec is gradual increases 1.0681 $\times 10^9$ at Time 1 sec.



(zirconium) Thermal Error V/s Time

V. CONCLUSION

By observing the above results are obtained from the thermal analysis of engine exhaust heat shield using high thermal conductivity and good thermal behavior of materials like STEEL 1008, Aluminium alloy, Zirconium

- From the above results observing high temperature obtained zirconium 8081.1 °C lowest materials is Aluminium alloy 3373.8 °C
- Highest Maximum heat flux obtained Aluminium alloy 370.98 W/mm² and lowest is zirconium 170.36 W/mm²
- Lowest thermal error occurring materials zirconium 1.0681 $\times 10^9$ and highest values is steel 1008 3.8314 $\times 10^9$

From this results from ovary materials having their thermal behavior and in this project mainly focused to analyze the better material for a heat shield for engine exhaust system so above results the better material for heat shield is zirconium to withstanding in the highest temperature comparing with other materials.

VI. FUTURE SCOPE

Today, heat protection (or thermal management) is not seen anymore as an isolated issue. In a total system approach, the applied heat shields are increasingly integrated into multifunctional components. Aluminum alloy, zirconium, steel alloy heat shields will be more and more integrated into innovativutions. Engine encapsulations to reduce fuel consumption and polluting emissions while treating noise at its source



- Combined heat protection and sound management solutions for the engine and exhaust line
- Thermal comfort in light vehicle passenger compartments. Acoustic heat shields combine effective thermal protection with a clear reduction in external noise. Underbody heat shields can also be considered as an integral component of the underbody system itself and even contribute to an improvement of the underbody aerodynamics. These latest products are commonplace in top-end motorsports such as Formula -1 cars.



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