

Application of Symbolic Regression in Modeling Soil Deformation Modulus



Vishweshwaran M, Anandha Kumar S

Abstract: It is not simple to determine in-situ horizontal stresses even though vertical stresses could be determined directly. Pressuremeter is not given high importance even though it is useful in illustrating various geotechnical parameters effectively. It is important to characterize geomaterials which in turn helps us to understand the properties and behavior of the materials. Symbolic Regression model has been prepared to relate pressuremeter test results with geotechnical engineering properties. Understandingthese properties help geotechnical engineers in design and analyses of foundations, earth pressures, etc.

Keywords: Symbolic regression, Genetic programming, Pressuremeter, Geotechnical properties, Geotechnical model.

I. INTRODUCTION

Pressuremeter test helps in determining angle of dilation for cohesionless soils, angle of internal friction for cohesionless soils, compressibility of a soil, undrained strength of cohesive soils, horizontal. It is imperative that the installation of pressuremeter contributes to the correctness of the results to be obtained. In order to install it to the very best quality, standardization of the installation methodology is required. Calibration of the instrument and measurements are to be done accurately. Pressuremeters represent cylindrical devices which apply unvarying, undifferentiated stresses to the surrounding walls of a borehole. Measurement of applied stresses and the deformation is the chief requirement for pressuremeter tests. In order to establish pressuremeter as a commonly used device, its accuracy and reliability in determination of its parameters from the in situ tests are preferable.

II. IMPORTANCE OF PRESSUREMETER TEST

Laboratory tests could be prone to more errors due to the disturbances of soil from its in situ state and the determination of engineering properties by cutting edge facilities may not be economical and may even delay the schedule of a project. Due to the factors such as flexible membrane features, differences in heights, compressibility, corrections are to be applied to the values of stress, lateral deformation and volume.

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Pressuremeter was initially used as an empirical measurement device but due to the requirements of good field data, the importance of pressuremeter is inevitable. Moreover, the in situ soils' boundary conditions are difficult to replicate in the laboratory in terms of load and deformation. In situ tests are equally important when compared to laboratory tests to analyze the properties of soils comprehensively. In situ pressuremeter tests have in recent years come into wide use in the determination of the parameters to be used for foundation design [1]. Model factor for evaluation of bearing capacity of piles in ultimate limit state is possible by Menard's pressuremeter test results [2]. It is possible to design laterally loaded piles with the help of P-y curve which could be obtained from pressuremeter curve. [3]. Response of the model with respect to predictor variable shall be analysed by parametric analysis. The robustness of a design equation is determined by examining how well the predicted target values agree with the underlying physical behavior of the investigated system [4]. The typical manner in which a pressuremeter is installed is installing vertically at various depths in the ground, and connected by tubing or cables to a control unit at the ground surface. There are various types of pressuremeters and all methods of interpretation of pressuremeter test results assume that the expanding cavity is sufficiently long for the deformation to be considered as cylindrical. A major difference between categories of pressuremeter tests lies in the method of installation of the pressuremeter device in the ground [5].

III. SYMBOLIC REGRESSION MODEL

Datasets for the model were selected from a literature of Jafar Bolouri Bazaz [6] and is presented in Table 1. Information on different particle sizes, soil classification parameters, moisture content, unit weights of the soil have been used in the datasets against secant modulus of the soil. The model aims in predicting equation for secant modulus based on the available geotechnical data. One of the principal benefits of using pressuremeter is the simultaneous measurement of deformation and strength. FC (%), D₁₀ (mm), D_{30} (mm), D_{60} (mm), C_u , C_c , LL (%), w (%), ρ_d (%) and E_p (kg/cm²) represent percentage of fines, particles sizes finer than 10%, 30%, 60%, coefficient of uniformity, coefficient of curvature, liquid limit, water content, dry density and secant modulus respectively. To utilize the search space in an efficient manner, evolutionary algorithm requires diversity because of which better performing models shall be created [1]. Response of the model with respect to predictor variable shall be analyzed by parametric analysis.



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The robustness of a design equation is determined by examining how well the predicted target values agree with the underlying physical behavior of the investigated system

Table- I: Dataset of geotechnical parameters and pressuremeter results [6]

| | Table- 1: Dataset of geotechnical parameters and pressuremeter results [6] | | | | | | | | | |
|------|--|-------------------|-----------------|-----------------|----------|----------------|---------------------------|----|---------------|--|
| S.No | FC (%) | \mathbf{D}_{10} | D ₃₀ | D ₆₀ | Cu | C _c | \mathbf{w}_{L} | W | $\rho_{ m d}$ | |
| 1 | 93.6 | 0.0007 | 0.0043 | 0.027 | 38.571 | 0.978 | 42 | 16 | 15.5 | |
| 2 | 71 | 0.0001 | 0.016 | 0.051 | 510.000 | 50.196 | 18 | 21 | 15.5 | |
| 3 | 97.0 | 0.0001 | 0.0003 | 0.007 | 70.000 | 0.129 | 40 | 22 | 15.5 | |
| 4 | 76.9 | 0.0008 | 0.0065 | 0.03 | 37.500 | 1.760 | 30 | 27 | 16.0 | |
| 5 | 94.0 | 0.0004 | 0.0011 | 0.024 | 60.000 | 0.126 | 28 | 20 | 15.5 | |
| 6 | 96.0 | 0.0001 | 0.007 | 0.014 | 140.000 | 35.000 | 35 | 22 | 15.5 | |
| 7 | 90.5 | 0.0001 | 0.0017 | 0.017 | 170.000 | 1.700 | 28 | 18 | 16.0 | |
| 8 | 98.0 | 0.0001 | 0.00017 | 0.012 | 120.000 | 0.024 | 17 | 18 | 16.0 | |
| 9 | 47.8 | 0.0001 | 0.025 | 0.28 | 2800.000 | 22.321 | 17 | 26 | 16.0 | |
| 10 | 17.6 | 0.013 | 0.48 | 1.5 | 115.385 | 11.815 | 17 | 26 | 16.0 | |
| 11 | 86.0 | 0.0001 | 0.003 | 0.02 | 200.000 | 4.500 | 17 | 26 | 16.0 | |
| 12 | 99.4 | 0.0001 | 0.011 | 0.031 | 310.000 | 39.032 | 27 | 18 | 16.5 | |
| 13 | 93.2 | 0.002 | 0.0084 | 0.025 | 12.500 | 1.411 | 34 | 17 | 17.8 | |
| 14 | 61.0 | 0.0017 | 0.024 | 0.07 | 41.176 | 4.840 | 33 | 22 | 15.3 | |
| 15 | 96.9 | 0.0007 | 0.007 | 0.022 | 31.429 | 3.182 | 34 | 10 | 17.5 | |
| 16 | 94.9 | 0.006 | 0.02 | 0.034 | 5.667 | 1.961 | 24 | 19 | 17.0 | |
| 17 | 86.6 | 0.0013 | 0.0073 | 0.035 | 26.923 | 1.171 | 31 | 15 | 17.0 | |
| 18 | 63.4 | 0.0029 | 0.021 | 0.064 | 22.069 | 2.376 | 23 | 12 | 19.8 | |
| 19 | 87.8 | 0.0012 | 0.017 | 0.03 | 25.000 | 8.028 | 25 | 17 | 16.9 | |
| 20 | 66.7 | 0.0029 | 0.0165 | 0.06 | 20.690 | 1.565 | 22 | 23 | 16.7 | |
| 21 | 87.8 | 0.0028 | 0.0115 | 0.035 | 12.500 | 1.349 | 26 | 17 | 17.8 | |
| 22 | 86.75 | 0.0018 | 0.0081 | 0.031 | 17.222 | 1.176 | 27 | 13 | 17.0 | |
| 23 | 92.75 | 0.0015 | 0.0085 | 0.025 | 16.667 | 1.927 | 34 | 13 | 17.0 | |
| 24 | 66.06 | 0.003 | 0.041 | 0.063 | 21.000 | 8.894 | 23 | 13 | 17.0 | |
| 25 | 93.66 | 0.0032 | 0.022 | 0.045 | 14.063 | 3.361 | 29 | 16 | 17.2 | |
| 26 | 83.85 | 0.0061 | 0.042 | 0.064 | 10.492 | 4.518 | 22 | 16 | 17.2 | |
| 27 | 80.44 | 0.0044 | 0.023 | 0.059 | 13.409 | 2.038 | 26 | 16 | 17.2 | |
| 28 | 91.39 | 0.0044 | 0.031 | 0.06 | 13.636 | 3.640 | 26 | 16 | 17.2 | |
| 29 | 97.0 | 0.0001 | 0.003 | 0.015 | 150.000 | 6.000 | 26 | 17 | 16.1 | |
| 30 | 52.0 | 0.0004 | 0.005 | 0.84 | 2100.000 | 0.074 | 21 | 20 | 16.8 | |
| 31 | 96.8 | 0.0011 | 0.004 | 0.021 | 19.091 | 0.693 | 20 | 19 | 16.1 | |
| 32 | 90.0 | 0.0006 | 0.001 | 0.017 | 28.333 | 0.098 | 32 | 19 | 16.3 | |
| 33 | 97.5 | 0.0007 | 0.0067 | 0.033 | 47.143 | 1.943 | 29 | 20 | 16.5 | |
| 34 | 71.7 | 0.0006 | 0.004 | 0.03 | 50.000 | 0.889 | 32 | 26 | 16.8 | |
| 35 | 86.5 | 0.0044 | 0.02 | 0.033 | 7.500 | 2.755 | 23 | 16 | 16.4 | |
| 36 | 80.0 | 0.0007 | 0.009 | 0.029 | 41.429 | 3.990 | 17 | 9 | 18.0 | |
| 37 | 81.4 | 0.0002 | 0.008 | 0.034 | 170.000 | 9.412 | 17 | 26 | 15.0 | |
| 38 | 59.0 | 0.0022 | 0.013 | 0.074 | 33.636 | 1.038 | 17 | 10 | 19.0 | |
| 39 | 32.5 | 0.0069 | 0.05 | 1.4 | 202.899 | 0.259 | 23 | 19 | 18.0 | |
| 40 | 47.8 | 0.0001 | 0.018 | 0.6 | 6000.000 | 5.400 | 23 | 14 | 16.2 | |
| 41 | 47.5 | 0.0003 | 0.018 | 0.95 | 3166.667 | 1.137 | 26 | 14 | 16.5 | |
| 42 | 94.6 | 0.0001 | 0.006 | 0.025 | 250.000 | 31.000 | 22 | 18 | 17.5 | |
| 43 | 12.3 | 0.007 | 0.9 | 6 | 857.143 | 19.286 | 16 | 6 | 14.6 | |
| 44 | 47.8 | 0.0001 | 0.013 | 0.7 | 7000.000 | 2.414 | 28 | 15 | 15.5 | |
| 45 | 56.7 | 0.0003 | 0.008 | 0.15 | 500.000 | 1.422 | 28 | 15 | 15.5 | |
| 46 | 92.0 | 0.0009 | 0.0071 | 0.02 | 22.222 | 2.801 | 27 | 15 | 15.5 | |
| 47 | 87.5 | 0.0005 | 0.0035 | 0.025 | 50.000 | 0.980 | 30 | 16 | 17.0 | |
| | | • | | | | | • | | | |

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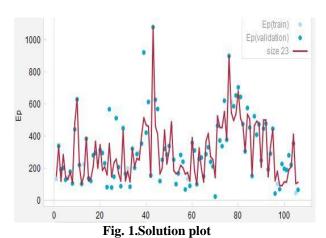


| 40 | 52.0 | 0.0005 | 0.014 | 0.17 | 340.000 | 2.206 | 22 | 1.0 | 17.0 |
|----|------|---------|---------|--------|----------|--------|----|-------|------|
| 48 | 52.0 | 010000 | 0.014 | 0.17 | | 2.306 | 23 | 16 | 17.0 |
| 49 | 84.5 | 0.0006 | 0.0015 | 0.018 | 30.000 | 0.208 | 36 | 14 | 14.5 |
| 50 | 73.4 | 0.0014 | 0.0114 | 0.04 | 28.571 | 2.321 | 31 | 18 | 14.3 |
| 51 | 40.0 | 0.0007 | 0.02 | 2.1 | 3000.000 | 0.272 | 28 | 14 | 17.5 |
| 52 | 89.6 | 0.0007 | 0.003 | 0.018 | 25.714 | 0.714 | 29 | 18 | 14.5 |
| 53 | 91.8 | 0.0006 | 0.0027 | 0.021 | 35.000 | 0.579 | 29 | 18 | 14.5 |
| 54 | 90.8 | 0.0012 | 0.009 | 0.024 | 20.000 | 2.813 | 35 | 18 | 14.5 |
| 55 | 86.0 | 0.0023 | 0.01 | 0.03 | 13.043 | 1.449 | 38 | 4 | 19.0 |
| 56 | 87.5 | 0.0004 | 0.0014 | 0.014 | 35.000 | 0.350 | 31 | 17 | 17.0 |
| 57 | 92.0 | 0.0004 | 0.0027 | 0.028 | 70.000 | 0.651 | 34 | 17 | 17.0 |
| 58 | 91.0 | 0.0002 | 0.005 | 0.028 | 140.000 | 4.464 | 17 | 18 | 17.5 |
| 59 | 97.0 | 0.0001 | 0.0012 | 0.02 | 200.000 | 0.720 | 31 | 18 | 17.5 |
| 60 | 60.0 | 0.0032 | 0.0215 | 0.073 | 22.813 | 1.979 | 18 | 15 | 17.5 |
| 61 | 89.6 | 0.0055 | 0.019 | 0.039 | 7.091 | 1.683 | 24 | 11 | 17.0 |
| 62 | 99.0 | 0.0012 | 0.011 | 0.029 | 24.167 | 3.477 | 28 | 17 | 17.0 |
| 63 | 71.0 | 0.001 | 0.013 | 0.063 | 63.000 | 2.683 | 30 | 17 | 17.0 |
| 64 | 88.4 | 0.00155 | 0.014 | 0.044 | 28.387 | 2.874 | 30 | 10 | 18.9 |
| 65 | 97.7 | 0.0015 | 0.0084 | 0.021 | 14.000 | 2.240 | 29 | 17 | 17.5 |
| 66 | 64.8 | 0.0021 | 0.014 | 0.06 | 28.571 | 1.556 | 23 | 16 | 17.5 |
| 67 | 56.0 | 0.0012 | 0.015 | 0.1 | 83.333 | 1.875 | 18 | 16 | 18.3 |
| 68 | 78.8 | 0.001 | 0.011 | 0.045 | 45.000 | 2.689 | 28 | 15 | 18.1 |
| 69 | 81.0 | 0.0006 | 0.0013 | 0.025 | 41.667 | 0.113 | 29 | 16 | 18.3 |
| 70 | 94.5 | 0.0005 | 0.004 | 0.021 | 42.000 | 1.524 | 28 | 17 | 18.5 |
| 71 | 33.0 | 0.0005 | 0.04 | 1.1 | 2200.000 | 2.909 | 17 | 17 | 18.5 |
| 72 | 49.2 | 0.013 | 0.051 | 0.11 | 8.462 | 1.819 | 20 | 14 | 18.9 |
| 73 | 48.0 | 0.004 | 0.02 | 0.25 | 62.500 | 0.400 | 17 | 12 | 18.0 |
| 74 | 20.0 | 0.02 | 0.21 | 0.595 | 29.750 | 3.706 | 17 | 12 | 18.0 |
| 75 | 62.5 | 0.0006 | 0.012 | 0.05 | 83.333 | 4.800 | 28 | 17 | 16.8 |
| 76 | 28.0 | 0.008 | 0.1 | 1.2 | 150.000 | 1.042 | 21 | 17 | 16.8 |
| 77 | 26.5 | 0.0056 | 0.15 | 1.3 | 232.143 | 3.091 | 21 | 17 | 18.0 |
| 78 | 37.5 | 0.0053 | 0.031 | 0.71 | 133.962 | 0.255 | 21 | 10 | 19.0 |
| 79 | 26.7 | 0.009 | 0.15 | 1.44 | 160.000 | 1.736 | 20 | 10 | 19.0 |
| 80 | 22.0 | 0.011 | 0.595 | 6 | 545.455 | 5.364 | 19 | 12 | 17.5 |
| 81 | 35.5 | 0.0009 | 0.04 | 1 | 1111.111 | 1.778 | 24 | 11 | 19.5 |
| 82 | 44.0 | 0.000 | 0.023 | 1.1 | 1100.000 | 0.481 | 17 | 7 | 19.0 |
| 83 | 74.4 | 0.0003 | 0.0095 | 0.03 | 100.000 | 10.028 | 24 | 15.94 | 19.5 |
| 84 | 30.0 | 0.0003 | 0.0033 | 2.2 | 1100.000 | 1.566 | 23 | 11 | 19.5 |
| 85 | 36.0 | 0.002 | 0.083 | 2.1 | 1909.091 | 0.693 | 23 | 11 | 19.5 |
| 86 | 93.0 | 0.0003 | 0.0042 | 0.012 | 40.000 | 4.900 | 39 | 4 | 19.0 |
| 87 | 45.0 | 0.0003 | 0.0042 | 0.012 | 242.424 | 0.064 | 23 | 4 | 19.0 |
| 88 | 38.0 | 0.0033 | 0.013 | 2 | 487.805 | 0.064 | 17 | 4 | 19.0 |
| 89 | 41.0 | 0.0041 | 0.022 | 1.3 | 317.073 | 0.039 | 17 | 4 | 19.0 |
| | | | | | | | | | |
| 90 | 87.0 | 0.00065 | 0.00477 | 0.0165 | 25.385 | 2.121 | 30 | 4 | 18.7 |
| 91 | 34.0 | 0.0044 | 0.05 | 9.7 | 2204.545 | 0.059 | 17 | 4 | 19.0 |
| 92 | 34.0 | 0.0045 | 0.05 | 9.6 | 2133.333 | 0.058 | 17 | 1.42 | 19.7 |
| 93 | 94.0 | 0.0007 | 0.0084 | 0.0215 | 30.714 | 4.688 | 35 | 3 | 19.0 |
| 94 | 70.0 | 0.00065 | 0.007 | 0.035 | 53.846 | 2.154 | 33 | 3 | 19.6 |
| 95 | 51.0 | 0.0006 | 0.011 | 0.6 | 1000.000 | 0.336 | 38 | 4 | 19.0 |
| 96 | 96.7 | 0.00006 | 0.0005 | 0.018 | 300.000 | 0.231 | 30 | 22 | 16.0 |
| 97 | 90.0 | 0.00005 | 0.0007 | 0.0138 | 276.000 | 0.710 | 32 | 22 | 16.0 |
| 98 | 99.9 | 0.0001 | 0.0008 | 0.014 | 140.000 | 0.457 | 32 | 22 | 16.0 |



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| 99 | 100.0 | 0.00008 | 0.00143 | 0.021 | 262.500 | 1.217 | 28 | 22 | 16.0 |
|-----|-------|---------|---------|--------|----------|--------|----|-------|------|
| 100 | 97.5 | 0.00007 | 0.0005 | 0.015 | 214.286 | 0.238 | 29 | 20 | 16.5 |
| 101 | 97.6 | 0.00007 | 0.00005 | 0.0115 | 164.286 | 0.003 | 34 | 20 | 16.5 |
| 102 | 88.8 | 0.0001 | 0.0022 | 0.023 | 230.000 | 2.104 | 27 | 20 | 16.5 |
| 103 | 86.8 | 0.0003 | 0.0035 | 0.022 | 73.333 | 1.856 | 29 | 20.85 | 16.0 |
| 104 | 56.5 | 0.00065 | 0.0021 | 2 | 3076.923 | 0.003 | 31 | 24 | 16.0 |
| 105 | 98.7 | 0.0007 | 0.0053 | 0.014 | 20.000 | 2.866 | 29 | 18 | 15.5 |
| 106 | 98.0 | 0.0004 | 0.014 | 0.03 | 75.000 | 16.333 | 23 | 17 | 16.5 |



Frontier 150 140 Solutions 130 size 23 120 110 100 90 80 70 60 25 30 0 5 10 15 20 Complexity

Fig. 2. Accuracy vs Complexity plot

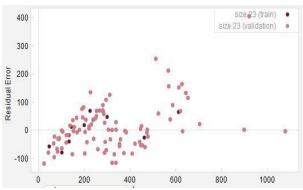


Fig. 3. Residual error plot

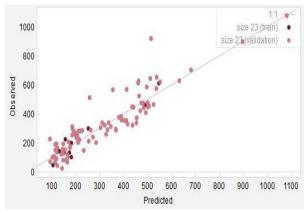


Fig. 4. Observed vs predicted plot

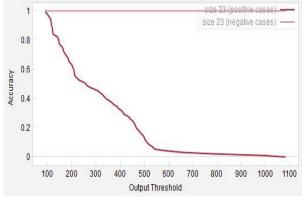


Fig. 5. Classification Threshold plot

IV. RESULTS AND DISCUSSION

$$E_p = 562.81 + 4.58 * D_{60} * C_c + tan (588.71 * D_{10}) - D_{60} - 0.047 * FC^2$$

The above equation indicates that effective size of the soil (D_{10}) , D_{60} and coefficient of curvature (C_c) result in positive values for secant modulus. Amount of fines, liquid limit, water content, coefficient of uniformity parameters do not contribute to the effectiveness of the secant modulus of pressuremeter test. Coefficient of determination (R^2) of the model indicating the goodness of fit is 0.829 with a mean average error of 58.48. Plots for solution, complexity, residual error, accuracy, classification threshold are shown in the figures.





V. CONCLUSION

The result shows that symbolic regression is a satisfactory tool for modeling complex geotechnical data. More number of datasets and more input parameters for different soils may increase the effectiveness of the model. Sensitivity analysis, parametric analysis may be further conducted to check and enhance the robustness of the obtained model. Deformation modulus of the soil is a very important field parameter and the reliability of the result may be useful in future analyses, design purposes, etc. The model shall also be used for cross verification for problematic soils.

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chapters. He has an academic experience of 3 years. He believes that environmental friendly practices in geotechnical engineering are very important in the future. He also believes that an inter-disciplinary approach is required in efficient and environmental friendly waste management issues. Geo-Environmental Engineering deals with engineering solutions relating to environmental impacts of contaminants within soils, and includes such aspects as understanding the migration, interactions and fate of contaminants, the protection of uncontaminated regions, the remediation or clean-up of contaminated sites.



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