Performance of Space Vector PWM based Induction Motor Drive using dspace


Abstract— A discontinuous space vector pulse width modulation (DSVPWM) is presented for v/f control of the induction motor drive to reduce common mode voltage (CMV). The continuous space vector pulse width modulation (SVPWM) algorithms use two zero state voltage vectors at the beginning and end of the switching pattern. More ever SVPWM generate more CMV at zero voltage vectors whereas in active zero state pulse width modulation (AZSPWM) algorithms CMV is minimized because of effective zero state voltage vectors. However SVPWM and AZSPWM algorithms use both zero voltage vectors at a time. The proposed DSVPWM based induction motor drive use only one zero voltage vector at a time reducing switching losses and harmonics in output phase voltages and currents. Experimental studies have been carried out for SVPWM, AZSPWM and DSVPWM based induction motor drive in dspace environment and results are presented.

Keywords- SVPWM, AZSPWM, common mode voltage, DSVPWM, zero voltage vectors.

I. INTRODUCTION

Induction motor drives in variable speed applications are getting popular because of developments in pulse width modulation (PWM) switching strategies [1]. The dynamic behavior induction motor drive with space vector pulse width modulation (SVPWM) is of interest by many researchers for medium and large scale industrial applications. The advantages of induction motor drives are replacing the DC motor drives in variable speed applications [2].

The low cost and simple construction of induction motor drives have to be operated with constant air gap flux which is achieved by changing supply voltage and frequency simultaneously. The working of the PWM inverters by several conventional PWM algorithms are discussed in [3]. The drawbacks of basic PWM techniques such as low DC bus utilization, variable switching frequency of the inverter and high value of lower order harmonics elevates the use of SVPWM inverters [4-8]. This can be carried out by SVPWM based voltage source inverters. SVPWM algorithm gives high quality of output voltage as the reference vector is synthesized by the nearest active and zero voltage vectors surrounding it in a sector. The sector identification is done by the angle calculation of reference voltage vector. The drawback of the SVPWM algorithm is it generates more CMV variations which cause bearing failure of the induction motor and electromagnetic interference with nearby equipment. Various hybrid filters has to be used to reduce the CMV [9-13]. This additional hardware equipment increase the cost and weight and leads to the complexity of the drive system. There are several algorithms which are designed to reduce the CMV and they are presented in [14-24]. The reduced common mode voltage PWM (RCMCPWM) algorithm avoids the use of zero voltage vectors which leads to the reduction of CMV. The different RCMCPWM algorithms are AZSPWM, remote state PWM (RS PWM) and near state PWM (NSPWM) [20-24]. Among all AZSPWM algorithms use simplified approach to create effective zero state voltage vector. It uses two active voltage vectors with equal times which are in opposite to each other. The AZSPWM algorithms use instantaneous phase voltages to calculate switching times. It generates high harmonic variations. SVPWM algorithm has less total harmonic distortion (THD) but generates high CMV whereas AZSPWM algorithms give lower CMV but generates high THD. The limitations of both SVPWM and AZSPWM algorithms can be avoided by implementing discontinuous space vector PWM (DSVPWM) algorithm. DSVPWM uses only one zero voltage vector at a time in entire switching pattern to reduce CMV and THD.

This paper presents the performance of the conventional induction motor drive by SVPWM, AZSPWM and DSVPWM algorithms and the results are plotted for the phase voltage, phase current, CMV and THD. The experiments are carried out on 1 HP, 410 V, 5 A, 1470 RPM induction motor using real time dspace interface.

II. CONVENTIONAL SVPWM AND AZSPWM ALGORITHMS

The drive is operated in v/f control maintaining constant air gap flux. Initially induction motor is operated by SVPWM inverter giving two level output phase voltage. Inverter output frequency is controlled by varying the modulation index (Mi). The block diagram of induction motor by SVPWM inverter is shown in Fig. 1. The SVPWM inverter produces 8 voltage vectors V0, V1 through V7 among V0 and V7 are zero voltage vectors as shown in Fig. 2. The reference voltage vector (V_ref) which is falling in any one of the six sectors can
Fig. 1 Block diagram of dspace based space vector based induction motor drive

be synthesized by volt-sec balance principle considering Ts as sampling time period.

By using (1), the voltage vector times for sector-I are calculated as in (2), (3) and (4).

\[ V_{ref}T_s = V_1T_1 + V_2T_2 + V_3T_3 + V_4T_4 \]  \hspace{1cm} (1)

\[ T_1 = \frac{2\sqrt{3}}{\pi}M_i \cdot \sin(60 - \alpha) \cdot T_s \]  \hspace{1cm} (2)

\[ T_2 = \frac{2\sqrt{3}}{\pi}M_i \cdot \sin \alpha \cdot T_s \]  \hspace{1cm} (3)

\[ T_s = T_3 - T_1 - T_2 \]  \hspace{1cm} (4)

The modulation index \((M_i)\) is calculated as \(M_i = \pi V_{ref} \sqrt{2} V_{dc}\). The inverter pole voltages and CMV calculation for total 8 switching states are given in Table. 1.

The CMV is the potential difference between the load neutral and the negative terminal of the DC bus and is represented as in (5).

\[ V_{com} = \frac{V_{a0} + V_{b0} + V_{c0}}{3} \]  \hspace{1cm} (5)

As observed from Table. 1. The magnitude of CMV depends on switching states selected, and the use of zero switching states give more CMV. In order to reduce CMV the use of direct zero state vectors is avoided and instead of that effective zero voltage vectors are created which results in active zero state pulse width modulation (AZSPWM) algorithms. The different configurations of AZSPWM algorithms according to how the zero state voltage vectors are created are classified as AZSPWM1, AZSPWM2 and AZSPWM3 algorithms.

**Table I. pole voltages and cmv of the svpwm inverter**

<table>
<thead>
<tr>
<th>Switching state</th>
<th>Inverter pole voltages</th>
<th>( V_{com} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>( V_0(000) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/2</td>
</tr>
<tr>
<td>( V_1(100) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_2(110) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_3(010) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_4(011) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_5(001) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_6(111) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/6</td>
</tr>
<tr>
<td>( V_7(111) )</td>
<td>( V_{a0} ) - ( V_{dc} )/2, ( V_{b0} ) - ( V_{dc} )/2, ( V_{c0} ) - ( V_{dc} )/2</td>
<td>( -V_{dc} )/2</td>
</tr>
</tbody>
</table>

In SVPWM algorithm for every 600 rotation of a reference vector in space vector hexagon the two adjacent active vectors and two zero voltage vectors are synthesized where as in AZSPWM algorithms active vectors remain same but instead of zero voltage vectors any one of the three combinations \( V_1-V4, V_2-V5 \) or \( V_3-V6 \) can be used. The generation of three AZSPWM algorithms are shown in Fig. 4. The switching times of the space vectors are calculated from the instantaneous phase voltages are given as (6).

\[
V_{an} = V_{ref} \cos(\theta)
\]

\[
V_{bn} = V_{ref} \cos\left(\theta - \frac{2\pi}{3}\right)
\]

\[
V_{cn} = V_{ref} \cos\left(\theta - \frac{4\pi}{3}\right)
\]

Then, at each instant, the high (\( V_{max} \)), medium (\( V_{mid} \)) and lower (\( V_{min} \)) values of 3-phase voltages are calculated and the switching times are derived as (7).

\[
T_1 = \frac{T_s}{V_{dc}} (V_{max} - V_{min})
\]

\[
T_2 = \frac{T_s}{V_{dc}} (V_{mid} - V_{min})
\]

**Fig. 2 Voltage space vectors of a SVPWM inverter**
Then, by using the space vector concept, the favorable switching sequences are calculated as illustrated in Table 2.

Table 2. Switching Pattern for active zero state Algorithms

<table>
<thead>
<tr>
<th>SECTOR</th>
<th>SVPWM</th>
<th>AZSPWM1</th>
<th>AZSPWM2</th>
<th>AZSPWM3</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0127-7210</td>
<td>3216-6123</td>
<td>5122-2215</td>
<td>4211-1124</td>
</tr>
<tr>
<td>2</td>
<td>0327-7230</td>
<td>4321-1234</td>
<td>6233-3326</td>
<td>5322-2235</td>
</tr>
<tr>
<td>3</td>
<td>0347-7430</td>
<td>5432-2345</td>
<td>1344-4431</td>
<td>6433-3346</td>
</tr>
<tr>
<td>4</td>
<td>0547-7450</td>
<td>6543-3456</td>
<td>2455-5542</td>
<td>1544-4451</td>
</tr>
<tr>
<td>5</td>
<td>0567-7650</td>
<td>1654-4561</td>
<td>3566-6653</td>
<td>2655-5562</td>
</tr>
<tr>
<td>6</td>
<td>0167-7610</td>
<td>2165-5612</td>
<td>4611-1164</td>
<td>3166-6613</td>
</tr>
</tbody>
</table>

Fig. 3 Voltage space vectors distribution of AZSPWM algorithms

III. PROPOSED DISCONTINUOUS SVPWM BASED INDUCTION MOTOR

In the present discontinuous SVPWM the zero voltage vectors are not combinely used, only one of it is used at a time. There is no change in active voltage vector times. The zero state vector time is divided as $T_{01}$ and $T_{02}$ and their expressions are derived and shown as (8).

$$T_0 = T_1 - T_2$$

$$T_{01} = a_0 T_0$$

$$T_{02} = (1 - a_0) T_0$$

The switching states of the voltage vectors are shown in Table 3.

Table 3. Switching Sequences for DSVPWM Algorithms

<table>
<thead>
<tr>
<th>Sector</th>
<th>DSVPWM</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>721-127</td>
</tr>
<tr>
<td>2</td>
<td>832-238</td>
</tr>
<tr>
<td>3</td>
<td>743-347</td>
</tr>
<tr>
<td>4</td>
<td>854-458</td>
</tr>
<tr>
<td>5</td>
<td>765-567</td>
</tr>
<tr>
<td>6</td>
<td>816-618</td>
</tr>
</tbody>
</table>

From eq (8) the value of $a_0$ is either 0 or 1. The value of $a_0$ in all sectors to generate discontinuous SVPWM is shown in Table 4.

Table 4. VALUE OF $a_0$ IN ALL SECTORS BY DSVPWM ALGORITHM

<table>
<thead>
<tr>
<th>Sector</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
</tr>
</thead>
<tbody>
<tr>
<td>$a_0$</td>
<td>1</td>
<td>0</td>
<td>0</td>
<td>1</td>
<td>1</td>
<td>0</td>
</tr>
</tbody>
</table>

In sector –1 from 0 to 300 the value of $a_0$ is 0 and then it is 0 from 300 to 600 and for the remaining sectors it is shown in Table 4.

IV. EXPERIMENTAL RESULTS AND DISCUSSIONS

To evaluate the performance of conventional induction motor drive in v/f control experimental studies have been done on various PWM algorithms. The gating signals to the PWM inverter is given by the dspace. The experimental setup is shown in the following figure. The control signals to the inverter are generated at a switching frequency of 3K Hz. The induction motor parameters are 1 HP, 440V, 5A, 1470 rpm.
The results of phase voltage, current, CMV variations phase current and voltage THD for SVPWM, AZSPWM1, AZSPWM2, AZSPWM3 and DSVPWM algorithms are shown in Fig. 4, Fig. 5, Fig. 6, Fig. 7 and Fig. 8 respectively.

V. CONCLUSIONS

DSVPWM based conventional induction motor drive has good performance. It produces output phase voltage and current with less THD comparing with continuous SVPWM and different configurations of AZSPWM algorithms. In proposed DSVPWM one zero switching state is avoided in one sampling time period resulting in reducing the switching losses of the inverter.

REFERENCES


