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Abstract: Safety concern in a vehicle plays a major role in development of any vehicle. Hence each and every vehicle has been studied in order to meet their safety requirement. In which, braking system is one of the major concern in safety as well as during breaking the heat is rejected to environment which leads to increase of global temperature. In this paper, the study of thermal analysis is carried out in rotor type disc brake with design modification as with and without cross drilled holes for various types of materials such as stainless steel, cast iron and aluminium alloy. Disc brakes are exposed to large thermal stresses during routine braking and extraordinary thermal stresses during hard braking. In order to overcome the thermal stress, disc brake rotor type is designed with cross drilled hole. The design is carried out by using CATIA V5 R21 and thermal analysis is carried out by using ANSYS. The result shows that the aluminium material with cross drilled hole has high thermal capacity for braking system among the other two materials such as cast iron and stainless steel.

Keywords: Disc brake, Temperature gradient, Thermal flux, Cross drilled hole, Different materials.

I. INTRODUCTION

The failure of braking system will leads to disastrous. So, consideration of braking system is most important. The basic principle behind the braking system is, it will coverts momentum into heat that is, and it will converts kinetic energy into thermal energy [6]. When car is under motion, the force which is applied will convert into a force ten times greater than an applied force. So, due to this brakes can be affected by thousands of pounds of pressure due to braking system. The thermal analysis of disc brake with rotor type is carried out by FEM method [10].

The basic components of braking systems are master cylinder – situated under hood and it is directly connected to brake pedal in which converts mechanical pressure into the hydraulic pressure. Brake lines made up of steel and flexible brake hoses are used to connect the master cylinder to slave cylinder, which is located at each wheel, where brake fluid is used. Drag force is created in order to slow down the car by pushing the shoes and pads to connect the drum and rotors by slave cylinder. Drum type doesn't exists sufficient resistance for brake fad but rotor type has a sufficient resistance to overcome brake fade [5]. Ventilation cannot be achieved greatly in the drum brakes. It can be achieved better in disk brakes [3]. Disc is connected either in wheels or axle.

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Warping, scarring, cracking and rusting are the major damaging modes. In most of the service shops, the new discs is provided if the cost of new disc is lower than the cost of resurfacing the old disk. Warping - the excessive heat will causes warping. When the friction area is at substantially higher temperature than inner portion, it will leads to greater thermal expansion in inner portion in which warping occurs and it can be minimized by floating [8].

Scarring is the brake pedal are not changed periodically, there will be considerable worn out and scarring occurs. In order to overcome scarring, prompt check-up of brake pads is necessary. Cracking is due to drilling the disc. Hairline cracks are occurs in cross drilled metal disc due to large amount of heat stored in disc. The only way to overcome cracking is changing the disc, if crack occurs in the disc. Disc is made up of cast iron as shown in Fig.1, it will raises to surface rust. In order to overcome rusting, the contact area of brake pads are kept clean by regular usage [7].



Fig. 1 Four wheeler disc brake

II. MATERIALS AND METHODS

In order to overcome the cost and safety concern, the selection of best material will play a vital role. In this paper, three materials are selected such as stainless steel, cast iron and aluminium alloy because of their own individual properties. The density of stainless steel, cast iron and aluminium alloy are 7612, 7100 and 2810 $\rm Kg/m^3$ respectively.

The properties of stainless steel have important features such as Aesthetics, Resistance to fire, Corrosion resistance, and clean ability. Whereas cast iron have some features like strong in compression and weak in tension, good fluidity, hard and little brittle, and shrinks on cooling and finally low melting point and aluminium alloy having some features like good corrosion resistance [9].

III. DESIGN OF DISK BRAKE

There are two types of design namely, disc with cross drilled hole and without



cross drilled hole, in which these two types of design is analyzed under various material. The weight of the cross drilled hole and without cross drilled holes are 2.58 kg and 2.733 kg. The design of disc is done by CATIA software, the thermal analysis of disc brake is carried out by ANSYS. Temperature distribution and other related thermal quantities are calculated by thermal analysis. Temperature distributions, temperature gradient, Thermal fluxes and amount of heat lost or gained is the main quantities of interest [4]. Thermal analysis is used to calculate the thermal stress by many engineers, thermal stress is a stress caused by thermal expansions or contractions. Fig.4 Stress variation of Tubular Tow Pin

IV. RESULT AND DISCUSSION

Thermal analysis of disc break with and without cross drilled holes for different material properties like Stainless steel, cast iron and aluminium alloy were done after meshing the component in tetrahedral mesh type. Nodal temperature, thermal flux & temperature gradient for each material property were determined.

A Thermal analysis of Stainless steel

Thermal analysis of disc break without cross drilled holes for Stainless steel was done and the maximum nodal temperature occurred was 353 K as shown in Fig.2. Thermal analysis of disc break with cross drilled holes for Stainless steel was done and the maximum nodal temperature occurred was 353 K as shown in Fig.3

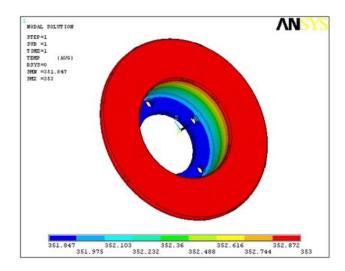


Fig.2 Nodal Temperature without holes

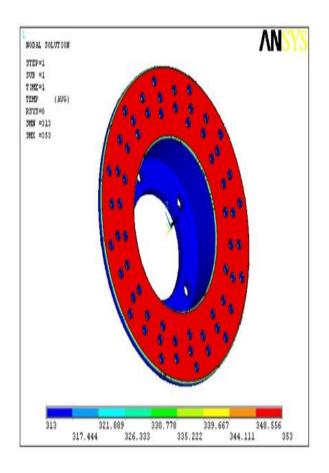


Fig.3 Nodal Temperature with holes

Thermal analysis of disc break without cross drilled holes for Stainless steel was done and the maximum temperature gradient was 84.381 K/mm as shown in Fig 4. Thermal analysis of disc break with cross drilled holes for Stainless steel was done and the maximum temperature gradient was 99.08 K/mm as shown in Fig 5.

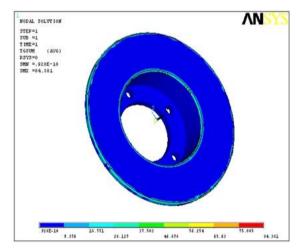


Fig.4 Temperature gradient without holes



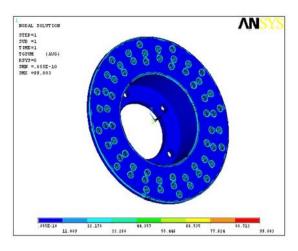


Fig.5 Temperature gradient with holes

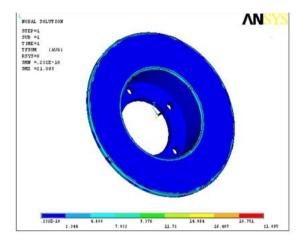


Fig.6 Thermal flux without holes

Thermal analysis of disc break without cross drilled holes for Stainless steel was done and the maximum thermal flux was 21.095 W/mm²as shown in Fig.6. Thermal analysis of disc break without cross drilled holes for Stainless steel was done and the maximum thermal flux was 24.951 W/mm²as shown in Fig.7.

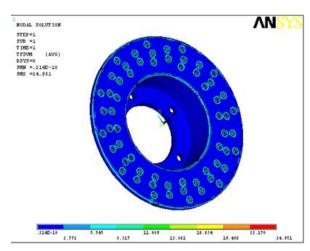


Fig.7 Thermal flux with holes

B. Thermal analysis of Cast Iron

Thermal analysis of disc break without cross drilled holes of cast iron was done and the maximum nodal temperature occurred was 353 K as shown in Fig.8. Thermal

analysis of disc break with cross drilled holes of cast iron was done and the maximum nodal temperature occurred was 353 K as shown in Fig.9. Thermal analysis of disc break without cross drilled holes of cast iron was done and the maximum temperature gradient was 98.891 K/mm as shown in Fig.10. Thermal analysis of disc break with cross drilled holes of cast iron was done and the maximum temperature gradient was 200.49 K/mm as shown in Fig.11.

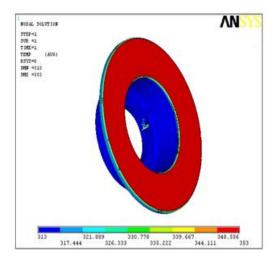


Fig.8 Nodal Temperature without holes

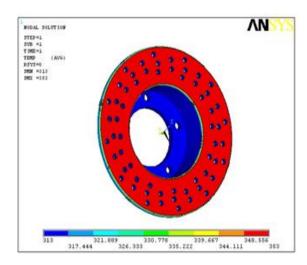


Fig.9 Nodal Temperature with holes

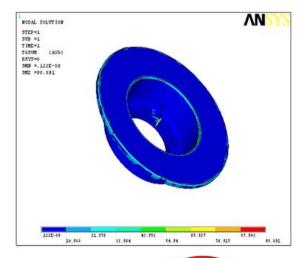


Fig.10 Temperature gradient without holes



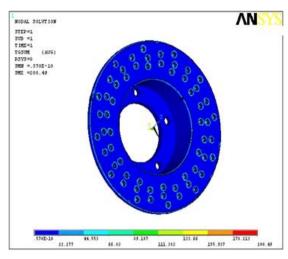


Fig.11 Temperature gradient with holes

Thermal analysis of disc break without cross drilled holes of cast iron was done and the maximum nodal temperature occurred was 353 K as shown in Fig.12. Thermal analysis of disc break with cross drilled holes of cast iron was done and the maximum thermal flux was 20.024 W/mm² as shown in Fig.13.

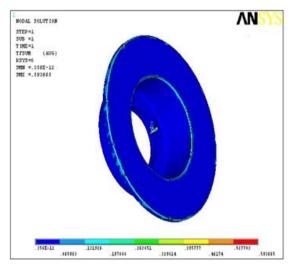


Fig.12 Thermal flux without holes

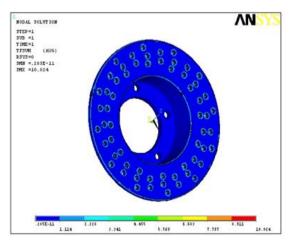


Fig.13 Thermal flux with holes

C. Thermal analysis of Aluminium Alloy

Thermal analysis of disc break without cross drilled holes for Aluminium alloy was done and the maximum nodal temperature occurred was 353 K as shown in Fig.14. Thermal analysis of disc break with cross drilled holes for Aluminium alloy was done and the maximum nodal temperature occurred was 353 K as shown in Fig.15. Thermal analysis of disc break without cross drilled holes for Aluminium alloy was done and the maximum temperature gradient was 118.733 K/mm as shown in Fig.16. Thermal analysis of disc break with cross drilled holes for Aluminium alloy was done and the maximum temperature gradient was 220.033 K/mm as shown in Fig.17. Thermal analysis of disc break without cross drilled holes for Aluminium alloy was done and the maximum thermal flux was 11.175 W/mm² as shown in Fig.18. Thermal analysis of disc break with cross drilled holes for Aluminium alloy was done and the maximum thermal flux was 24.864 W/mm² as shown in Fig.19

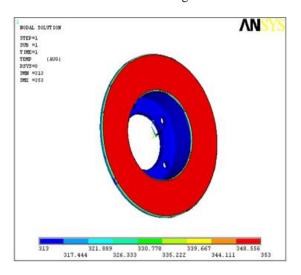


Fig.14 Nodal Temperature without holes

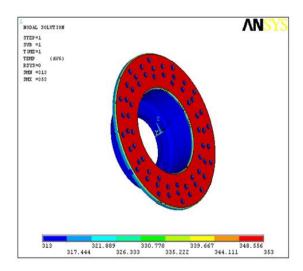


Fig.15 Nodal Temperature without holes



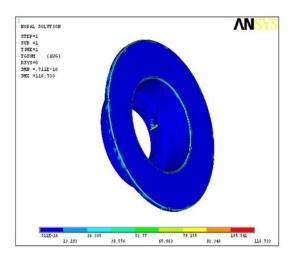


Fig. 16 Temperature gradient without holes

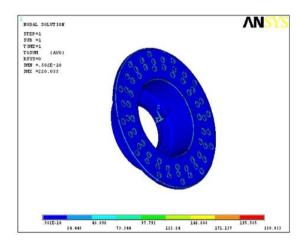


Fig.17 Temperature gradient with hole

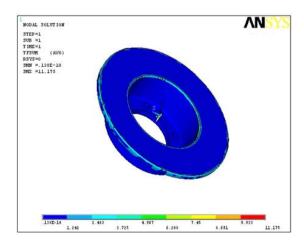


Fig.18 Thermal flux without holes

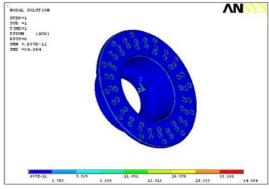


Fig.19 Thermal flux with holes

D. Comparison of thermal analysis

The comparison results of thermal analysis in which nodal temperature, temperature gradient and thermal flux are given in Table.1. The results of disc brake without cross drilled holes are given in which nodal temperature is same for every material and temperature gradient is high in cast iron as 198.89 k/mm and thermal flux is high for stainless steel as 21.095 W/mm². The thermal flux of cast iron is very high compared to other two materials hence it can be used as a disc brake material.

Table 1 Thermal analysis of disc brake without holes.

Analysis	Stainless	Cast	Aluminium
	Steel	Iron	Alloy
Nodal Temperature (K)	353	353	353
Temperature Gradient (K/mm)	84.38	198.8 9	118.73
Thermal Flux (W/mm ²)	21.09	0.593	11.17

In Table 2, results of disc brake with cross drilled holes are given in which nodal temperature is same for all the material and temperature gradient is high for aluminium as 220.33 k/mm and thermal flux is same for stainless steel as well as aluminium as 24.85 W/mm² approximately.

Table 2 Thermal analysis of disc brake with holes.

Analysis	Stainless Steel	Cast Iron	Aluminium Alloy
Nodal Temperature (K)	353	353	353
Temperature Gradient (K/mm)	99.803	200.49	220.33
Thermal Flux (W/mm ²)	24.951	20.024	24.864



The comparison results between with and without cross drilled hole, the aluminium with holes disc brake gives the better results than the other materials. As well as comparison of weight between the materials, aluminium seems to be unique feature. That is the weight is less for aluminium with cross drilled holes disk. The aluminium with cross drilled holes disk brake is selected.

Table 3 Weight of various materials

Material	Weight (G)	Weight (G)	
	Without Cross	With Cross	
	Drilled Holes	Drilled Holes	
Stainless Steel	2733	2580	
Cast Iron	2590	2336	
Aluminum Alloy	1456	1246	

V. CONCLUSION

Thermal analysis for various materials such as stainless steel, cast iron and aluminium alloy is carried out. By observing thermal analysis results, temperature gradient is more for aluminium alloy that is heat transfer rate is more for aluminium alloy by comparing with other two materials. The design of disc brake is changed by adding holes. From the results, it seems that the aluminium has the property that can be used as disk material with cross drilled hole design in which weight is 1246kg and nodal temperature, temperature gradient and thermal flux are 353 k, 220.33 k/mm and 24.864 W/mm². By adding holes, temperature gradient has increased when compared with the present design. Hence by changing the design of disc brake the heat transfer rate increases and using aluminium alloy is better.

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