

Diffusion Coefficient for Sublimation Diffusion Of Disperse Dye using Error Function

Geon-Yong Park

Abstract This study on the sublimation diffusion of disperse dye from paste into PET film was performed by using a film roll method. The Laplace transform was applied to finding the solution of the diffusion equation for the diffusion in a semi-infinite medium. The process to calculate the diffusion coefficient using the iterated complementary error function was proposed. For the sublimation diffusion of disperse dye to PET by treating at 190°C for 3 hours, the mean dye concentration for each layer was determined colorimetrically and the diffusion coefficient was calculated by obtaining the variable value of the iterated complementary error function derived from the ratio of the mean dye concentrations between adjacent layers. The mean diffusion coefficient for all the layers was unsuitable because of its large standard deviation, while that for below the 5th layer was estimated to be appropriate. The surface concentration calculated by the equation of the iterated complementary error function for the third layer was suitable.

Keywords: Iterated complementary error function, Diffusion coefficient, Disperse dye, Laplace transform, PET, Sublimation

I. INTRODUCTION

In the dyeing and printing process of PET textiles with disperse dyes, it is imperative that as much of the vaporized disperse dye as possible can be absorbed by the polyester fibres. The diffusion coefficient of commercial disperse dyes are essential for the design of the sublimation processes such as vapor-phase dyeing[1], conventional printing[2,3], and sublimation transfer printing.[4,5] Sekido and Matsui[6] applied a film roll method to study the kinetic behaviour of vat dyes in cellulose substrate. Sicardi et al.[7,8] applied a film roll method to measure the diffusion coefficients of dyes to PET film in supercritical carbon dioxide. They proposed a method of determining surface concentration by means of allowing a flap of film to protrude from the outer layer of the roll and reaching this flap to dye saturation at the polymer-bath interface.

General solutions of the diffusion equation can be obtained for a variety of initial and boundary conditions provided the diffusion coefficient is constant. A solution of the diffusion equation usually has one of two standard forms, one of which is a series of error functions and the other is a trigonometrical series[9]. Laplace transformation is a mathematical device which is useful for the solution of various problems in mathematical physics. Application of the Laplace transform to the diffusion equation removes the

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time variable and reduces the partial differential equation to the ordinary differential equation. The solution of the diffusion equation yields the transform of the concentration as a function of distance, satisfying the initial and boundary conditions[10].

In this study, first of all, the Laplace transform was applied to finding the solution of the diffusion equation for the diffusion in a semi-infinite medium. The solving process of obtaining the equation of the iterated complementary error function for the calculation of the diffusion coefficient was explained and proposed[9]. When disperse dye in paste was treated at 190°C for 3 hours using a film roll method, the mean dye concentration was determined colorimetrically. The diffusion coefficient was calculated by obtaining the variable value of the iterated complementary error function from the ratio of the mean dye concentrations between adjacent layers. The surface concentrations were also calculated by the equation of the iterated complementary error function.

II. MATERIALS AND METHODS

2.1. Materials

C. I. Disperse Violet 26 (Sumicaron Bordeaux SE-BL) was used without further purification. Biaxially oriented polyethyleneterephthalate (PET) film (40 μm in thickness) was supplied by SKC. Sodium alginate was the first grade.

2.2. Preparation of film roll

The PET film of 40 μm in thickness, of which width is 4 cm and length is 50 cm, was wrapped tightly around a glass rod of 1 cm in diameter. Both sides of film roll were wrapped by aluminium tape of which thickness is 180 μm . Sodium alginate paste was composed of C. I. Disperse Violet 26 of 300 g and 5% (w/w) sodium alginate stock paste of 700 g. Sodium alginate paste containing disperse dye was coated on the film roll between both barriers of aluminium tape and dried sufficiently at 100°C in dryer. The top of roll was fixed firmly by a thin aluminium tape and cotton yarn with glass rod for dividing layers[11,12]. Figure 1 shows the schematic image of film roll method.



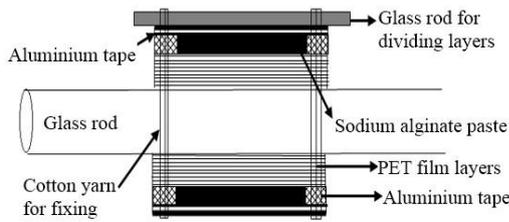


Figure 1. Image of film roll coated by paste containing dye

2.3. Heat treatment

The film roll coated with paste containing disperse dye was treated in laboratory curing chamber at 170-190°C for 3-4 hours for the sublimation of disperse dye. After heat treatment was finished, the film was unrolled, washed with water, and cut into the section pieces representing the successive layers.

2.4. Determination of dye concentration

These films of each layer were dipped in test tubes including chlorobenzene for the extraction of dye. The concentration of dye extracted from the section pieces was determined using spectrophotometer (Agilent Cary 8454).

III. RESULTS AND DISCUSSION

3.1. Application of Laplace transform

A film roll method was used to study the diffusion behaviour of disperse dye into PET film. The Laplace transform and a series of error functions can be applied to the diffusion equation to determine the diffusion coefficient and the surface concentration. If diffusion is one-dimensional and the diffusion coefficient (D) is a constant, the diffusion equation Eq. (1) is obtained by Fick's second law [13,14].

$$\frac{\partial C(x, t)}{\partial t} = D \frac{\partial^2 C(x, t)}{\partial x^2} \quad (1)$$

$C(x, t)$ is the concentration ($\text{mg}\cdot\text{cm}^{-3}$) at position x at time t . x is distance (cm) from surface of film roll. t is time (minute).

The dimension of D is $\text{cm}^2\cdot\text{min}^{-1}$.

$$\int_0^\infty e^{-pt} \frac{\partial C(x, t)}{\partial t} dt = [C(x, t)e^{-pt}]_0^\infty + p \int_0^\infty e^{-pt} C(t) dt = (0 - 0) + p\mathcal{C}(p) = p\mathcal{C}(p) \quad (8)$$

Also the right hand of Eq. (6) becomes the function of the Laplace transform $\mathcal{C}(x, t)$, i.e. Eq. (9).

$$D \int_0^\infty e^{-pt} \frac{\partial^2 C(x, t)}{\partial x^2} dt = D \frac{\partial^2}{\partial x^2} \int_0^\infty e^{-pt} C(t) dt = D \frac{\partial^2 \mathcal{C}(x, t)}{\partial x^2} \quad (9)$$

Thus Eq. (1) is reduced to Eq. (10) by combining Eq. (8) with Eq. (9).

$$p\mathcal{C}(p) = D \frac{\partial^2 \mathcal{C}(x, t)}{\partial x^2} \quad (10)$$

By treating the boundary condition Eq. (3), Eq. (11) is obtained [16].

$$\mathcal{C}(0, t) = \int_0^\infty e^{-pt} C(0, t) dt = \int_0^\infty e^{-pt} C_0 dt = \left[-\frac{C_0}{p} e^{-pt} \right]_0^\infty = 0 - \left(-\frac{C_0}{p} \right) = \frac{C_0}{p} \quad (11)$$

The Laplace transform reduces the partial differential equation to the ordinary differential equation (ODE) Eq. (12).

$$\frac{d^2 \mathcal{C}(x)}{dx^2} = \frac{p}{D} \mathcal{C}(x) \quad (12)$$

If a solution of ODE Eq. (12) is $C(x) = e^{\lambda x}$, a characteristic equation is Eq. (13).

$$\lambda^2 = \frac{p}{D} \quad (13)$$

The characteristic equation Eq. (13) has real roots, i.e. $\lambda = \pm \sqrt{p/D}$. Thus the general

Assuming that the PET film roll may be considered a semi-infinite medium in the direction of the center of the film roll, the surface concentration (C_0) at position $x = 0$ in one dimension of the x -axis is maintained at constant through the whole period of diffusing under the infinite dye-bath condition, and the initial concentration is zero throughout the medium, then the solution $C(x, t)$ of diffusion equation satisfies the initial condition Eq. (2) and the boundary conditions Eq. (3) and Eq. (4).

$$\text{Initial condition: } C(x, 0) = 0, \quad 0 < x < \infty \quad (2)$$

$$\text{Boundary conditions: } C(0, t) = C_0, \quad \forall t > 0 \quad (3)$$

$$C(\infty, t) = 0, \quad \forall t > 0 \quad (4)$$

To seek solutions of Eq (1), let $C(x, t) = C(p)$. Then a special solution of Eq. (1) is a function of one variable p as the form of Eq. (5).

$$C(x, t) = C(p) = C \left(\frac{x}{\sqrt{4Dt}} \right) \quad (5)$$

Multiplying both sides of Eq. (1) by e^{-pt} for the application of the Laplace transform and integrating with respect to t from 0 to ∞ yield Eq. (6).

$$\int_0^\infty e^{-pt} \frac{\partial C(x, t)}{\partial t} dt = D \int_0^\infty e^{-pt} \frac{\partial^2 C(x, t)}{\partial x^2} dt \quad (6)$$

The Laplace transform $\mathcal{C}(x, t)$ of $C(x, t)$ is defined as Eq. (7) [15].

$$\mathcal{C}(p) = \int_0^\infty e^{-pt} C(t) dt \quad (7)$$

Assuming that the orders of differentiation and integration can be interchanged, and integrating by parts, the left hand of Eq. (6) becomes Eq. (8). Since the term in the square bracket vanishes at $t = 0$ by virtue of the initial condition Eq. (2) and at $t = \infty$ through the exponential factor.

solution of ODE Eq. (12) is Eq. (14), where k_1 and k_2 are constants.

$$C(x) = k_1 e^{x\sqrt{p/D}} + k_2 e^{-x\sqrt{p/D}} \quad (14)$$

Because the solution of Eq. (12) must remain finite as x approaches infinity and satisfy Eq. (11), thus $k_1 = 0$ and $k_2 = C_0/p$. Thus the final solution of Eq. (12) is Eq. (15).

$$C(x) = \frac{C_0}{p} e^{-x\sqrt{p/D}} \quad (15)$$

3.2. Application of complementary error function

The error function $\text{erf}(z)$ is Eq. (16). The complementary error function $\text{erfc}(z)$ is Eq. (17).

$$\text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_0^z e^{-u^2} du \quad (16)$$

$$\text{erfc}(z) = 1 - \text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_z^\infty e^{-u^2} du \quad (17)$$

When $f(t) = \text{erfc}(z)$, the Laplace transform $f(p)$ of $f(t)$ is defined by Eq. (18).

$$f(p) = \int_0^\infty e^{-pt} f(t) dt = \int_0^\infty e^{-pt} \text{erfc}(z) dt \quad (18)$$

When $z = k/\sqrt{4t}$, the Laplace transform $f(p)$ of Eq. (18) is given by Eq. (19).

$$f(p) = \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-pt} \left(\int_z^\infty e^{-u^2} du \right) dt = \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-pt} \left(\int_{\frac{k}{\sqrt{4t}}}^\infty e^{-u^2} du \right) dt = \frac{2}{\sqrt{\pi}} \int_0^\infty \int_{\frac{k}{\sqrt{4t}}}^\infty e^{-pt} e^{-u^2} du dt \quad (19)$$

By changing the order of integration and noting that $u = k/\sqrt{4t}$ and $t = k^2/4u^2$, Eq. (20) is obtained.

$$\begin{aligned} f(p) &= \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-u^2} \left(\int_{\frac{k^2}{4u^2}}^\infty e^{-pt} dt \right) du = \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-u^2} \left[-\frac{1}{p} e^{-pt} \right]_{\frac{k^2}{4u^2}}^\infty du = \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-u^2} \left(0 + \frac{1}{p} e^{-\frac{k^2 p}{4u^2}} \right) du \\ &= \frac{2}{p\sqrt{\pi}} \int_0^\infty e^{-u^2} e^{-\frac{k^2 p}{4u^2}} du = \frac{2}{p\sqrt{\pi}} \int_0^\infty e^{-(u^2 + \frac{k^2 p}{4u^2})} du \quad (20) \end{aligned}$$

For solving the integral in Eq. (20), the derivatives of complementary error function, Eq. (21) and Eq. (22), are used.

$$\frac{\partial}{\partial u} \left[\text{erfc} \left(\frac{\sqrt{a}}{u} + u \right) \right] = \frac{2}{\sqrt{\pi}} e^{-\left(\frac{\sqrt{a}}{u} + u\right)^2} \left(\frac{\sqrt{a}}{u^2} - 1 \right) \quad (21)$$

$$\frac{\partial}{\partial u} \left[\text{erfc} \left(\frac{\sqrt{a}}{u} - u \right) \right] = \frac{2}{\sqrt{\pi}} e^{-\left(\frac{\sqrt{a}}{u} - u\right)^2} \left(1 + \frac{\sqrt{a}}{u^2} \right) \quad (22)$$

The integral in Eq. (20) can be converted into Eq. (23), of which the each integral term can be represented as Eq. (24) and Eq. (25) using Eq. (21) and Eq. (22). Thus Eq. (26) is obtained.

$$\int e^{-(u^2 + \frac{a}{u^2})} du = \frac{\sqrt{\pi}}{4} \int \frac{2e^{-\left(\frac{\sqrt{a}}{u} + u\right)^2 + 2\sqrt{a}} \left(1 - \frac{\sqrt{a}}{u^2} \right) + 2e^{-\left(\frac{\sqrt{a}}{u} - u\right)^2 - 2\sqrt{a}} \left(\frac{\sqrt{a}}{u^2} + 1 \right)}{\sqrt{\pi}} du \quad (23)$$

$$\int \frac{2e^{-\left(\frac{\sqrt{a}}{u} + u\right)^2 + 2\sqrt{a}} \left(1 - \frac{\sqrt{a}}{u^2} \right)}{\sqrt{\pi}} du = -e^{2\sqrt{a}} \frac{2}{\sqrt{\pi}} \int e^{-\left(\frac{\sqrt{a}}{u} + u\right)^2} \left(\frac{\sqrt{a}}{u^2} - 1 \right) du = e^{2\sqrt{a}} \left[-\text{erfc} \left(\frac{\sqrt{a}}{u} + u \right) \right] \quad (24)$$

$$\int \frac{2e^{-\left(\frac{\sqrt{a}}{u} - u\right)^2 - 2\sqrt{a}} \left(\frac{\sqrt{a}}{u^2} + 1 \right)}{\sqrt{\pi}} du = e^{-2\sqrt{a}} \frac{2}{\sqrt{\pi}} \int e^{-\left(\frac{\sqrt{a}}{u} - u\right)^2} \left(\frac{\sqrt{a}}{u^2} + 1 \right) du = e^{-2\sqrt{a}} \left[\text{erfc} \left(\frac{\sqrt{a}}{u} - u \right) \right] \quad (25)$$

$$\begin{aligned} \int e^{-(u^2 + \frac{a}{u^2})} du &= \frac{\sqrt{\pi}}{4} \left\{ e^{2\sqrt{a}} \left[-\text{erfc} \left(\frac{\sqrt{a}}{u} + u \right) \right] + e^{-2\sqrt{a}} \left[\text{erfc} \left(\frac{\sqrt{a}}{u} - u \right) \right] \right\} \\ &= \frac{\sqrt{\pi}}{4} \left\{ e^{2\sqrt{a}} \left[\text{erf} \left(\frac{\sqrt{a}}{u} + u \right) - 1 \right] + e^{-2\sqrt{a}} \left[1 - \text{erf} \left(\frac{\sqrt{a}}{u} - u \right) \right] \right\} \quad (26) \end{aligned}$$

The integral in Eq. (20) calculated by substituting $a = k^2 p/4$ in Eq. (26) is Eq. (27).



$$\int_0^{\infty} e^{-(u^2 + \frac{k^2 p}{4u^2})} du = \frac{\sqrt{\pi}}{4} \left[e^{k\sqrt{p}} \left\{ \operatorname{erf} \left(\frac{k\sqrt{p}}{2u} + u \right) - 1 \right\} + e^{-k\sqrt{p}} \left\{ 1 - \operatorname{erf} \left(\frac{k\sqrt{p}}{2u} - u \right) \right\} \right]_0^{\infty}$$

$$= \frac{\sqrt{\pi}}{4} \{ e^{k\sqrt{p}}(1 - 1 - 1 + 1) + e^{-k\sqrt{p}}(1 + 1 - 1 + 1) \} = \frac{\sqrt{\pi}}{2} e^{-k\sqrt{p}} \quad (27)$$

When $f(t) = \operatorname{erfc}(k/\sqrt{4t})$, the Laplace transform $f'(p)$ of $f(t)$ is defined by Eq. (28)[17].

$$f'(p) = \int_0^{\infty} e^{-pt} f(t) dt = \int_0^{\infty} e^{-pt} \operatorname{erfc} \left(\frac{k}{\sqrt{4t}} \right) dt = \frac{2}{p\sqrt{\pi}} \cdot \frac{\sqrt{\pi}}{2} e^{-k\sqrt{p}} = \frac{1}{p} e^{-k\sqrt{p}} \quad (28)$$

If the exponent $k\sqrt{p}$ in Eq. (28) is equal to the exponent $x\sqrt{p}/\sqrt{D}$ in Eq. (15), then $k = x/\sqrt{D}$. Thus the Laplace transform $\bar{C}(p)$ of Eq. (15) is rewritten in the form of Eq. (29) according to Eq. (28).

$$\bar{C}(p) = \int_0^{\infty} e^{-pt} C(t) dt = \frac{C_0}{p} e^{-\frac{p}{D}x} = C_0 \frac{1}{p} e^{-\frac{x}{\sqrt{D}}\sqrt{p}} = C_0 \int_0^{\infty} e^{-pt} \operatorname{erfc} \left(\frac{x}{\sqrt{4Dt}} \right) dt \quad (29)$$

Finally Eq. (30) can be obtained from Eq. (29).

$$C(x, t) = C_0 \operatorname{erfc} \left(\frac{x}{\sqrt{4Dt}} \right) \quad (30)$$

3.3. Iterated complementary error function

If $F(x)$ is an antiderivative of $C(x, t)$ for the integration of $C(x, t)$ with respect to x from 0 to x , then Eq. (31) is obtained.

$$F(x) = \int_0^x C(x, t) dx = \int_0^x C_0 \operatorname{erfc} \left(\frac{x}{\sqrt{4Dt}} \right) dx \quad (31)$$

The repeated integrals of the complementary error function, i.e. $i^n \operatorname{erfc}(z)$, are defined by Eq. (32)[18].

$$i^n \operatorname{erfc}(z) = \int_z^{\infty} i^{n-1} \operatorname{erfc}(\zeta) d\zeta = \frac{2}{\sqrt{\pi}} \int_z^{\infty} \frac{(\zeta - z)^n}{n!} e^{-\zeta^2} d\zeta \quad (32)$$

The repeated integral of the complementary error function for $n = 1$, i.e. $i \operatorname{erfc}(z)$ called the iterated complementary error function, is Eq. (35) which can be obtained from Eq. (33) and Eq. (34).

$$i \operatorname{erfc}(z) = \int_z^{\infty} i^0 \operatorname{erfc}(\zeta) d\zeta = \frac{2}{\sqrt{\pi}} \int_z^{\infty} (\zeta - z) e^{-\zeta^2} d\zeta = \frac{2}{\sqrt{\pi}} \int_z^{\infty} \zeta e^{-\zeta^2} d\zeta - z \operatorname{erfc}(z) \quad (33)$$

$$\frac{2}{\sqrt{\pi}} \int_z^{\infty} \zeta e^{-\zeta^2} d\zeta = \frac{2}{\sqrt{\pi}} \int_z^{\infty} \left(-\frac{1}{2} \right) e^{-\zeta^2} (-2\zeta) d\zeta = \left[-\frac{1}{\sqrt{\pi}} e^{-\zeta^2} \right]_z^{\infty} = \left(-0 + \frac{1}{\sqrt{\pi}} e^{-z^2} \right) = \frac{1}{\sqrt{\pi}} e^{-z^2} \quad (34)$$

$$i \operatorname{erfc}(z) = \int_z^{\infty} \operatorname{erfc}(\zeta) d\zeta = \frac{1}{\sqrt{\pi}} e^{-z^2} - z \operatorname{erfc}(z) \quad (35)$$

Substituting z for $x/\sqrt{4Dt}$ in Eq. (31) as Eq. (36) and combining Eq. (32) with Eq. (31) yield Eq. (38) through Eq. (37).

$$z = \frac{x}{\sqrt{4Dt}} \rightarrow dx = \sqrt{4Dt} dz \quad (36)$$

$$F(b) - F(a) = \int_a^b C(x, t) dx = C_0 \sqrt{4Dt} \int_{\frac{a}{\sqrt{4Dt}}}^{\frac{b}{\sqrt{4Dt}}} \operatorname{erfc}(z) dz = C_0 \sqrt{4Dt} \left(\int_{\frac{a}{\sqrt{4Dt}}}^{\infty} \operatorname{erfc}(z) dz - \int_{\frac{b}{\sqrt{4Dt}}}^{\infty} \operatorname{erfc}(z) dz \right) \quad (37)$$

$$\int_a^b C(x, t) dx = C_0 \sqrt{4Dt} \left\{ i \operatorname{erfc} \left(\frac{a}{\sqrt{4Dt}} \right) - i \operatorname{erfc} \left(\frac{b}{\sqrt{4Dt}} \right) \right\} \quad (38)$$

Let the mean concentration in i -th layer from the outside be \bar{C}_i and the thickness of each layer be ε . Then since the total concentration $\varepsilon \bar{C}_i$ in i -th layer is equal to the integration of $C(x, t)$ with respect to x from $(i-1)\varepsilon$ to $i\varepsilon$, Eq. (39) is obtained where $i = 1, 2, \dots, n$.

$$\varepsilon \bar{C}_i = F(i\varepsilon) - F((i-1)\varepsilon) = \int_{(i-1)\varepsilon}^{i\varepsilon} C(x, t) dx = C_0 \sqrt{4Dt} \left\{ i \operatorname{erfc} \left[\frac{(i-1)\varepsilon}{\sqrt{4Dt}} \right] - i \operatorname{erfc} \left(\frac{i\varepsilon}{\sqrt{4Dt}} \right) \right\} \quad (39)$$

Eq. (39) can be rewritten in the form of Eq. (40), where $\zeta = \varepsilon/\sqrt{4Dt}$.



$$\frac{\bar{C}_i}{C_0} = \frac{\sqrt{4Dt}}{\varepsilon} \left\{ \text{ierfc} \left[\frac{(i-1)\varepsilon}{\sqrt{4Dt}} \right] - \text{ierfc} \left(\frac{i\varepsilon}{\sqrt{4Dt}} \right) \right\} = \frac{1}{\zeta} \{ \text{ierfc}[(i-1)\zeta] - \text{ierfc}(i\zeta) \} \quad (40)$$

In the same way the mean concentration \bar{C}_{i+1} in $(i+1)$ -th layer divided by C_0 can be written in the form of Eq. (41).

$$\frac{\bar{C}_{i+1}}{C_0} = \frac{\sqrt{4Dt}}{\varepsilon} \left\{ \text{ierfc} \left(\frac{i\varepsilon}{\sqrt{4Dt}} \right) - \text{ierfc} \left(\frac{(i+1)\varepsilon}{\sqrt{4Dt}} \right) \right\} = \frac{1}{\zeta} \{ \text{ierfc}(i\zeta) - \text{ierfc}((i+1)\zeta) \} \quad (41)$$

Thus \bar{C}_{i+1}/\bar{C}_i of eq. (42) can be obtained from dividing Eq. (41) by Eq. (40).

$$\frac{\bar{C}_{i+1}}{\bar{C}_i} = \frac{\text{ierfc}(i\zeta) - \text{ierfc}((i+1)\zeta)}{\text{ierfc}[(i-1)\zeta] - \text{ierfc}(i\zeta)} \quad (42)$$

3.4. Diffusion coefficient

The diffusion coefficients were calculated by obtaining the values of ζ from eq. (42). The value of ζ was calculated by obtaining the ratio of \bar{C}_{i+1}/\bar{C}_i . The mean dye concentration was determined using spectrophotometer.

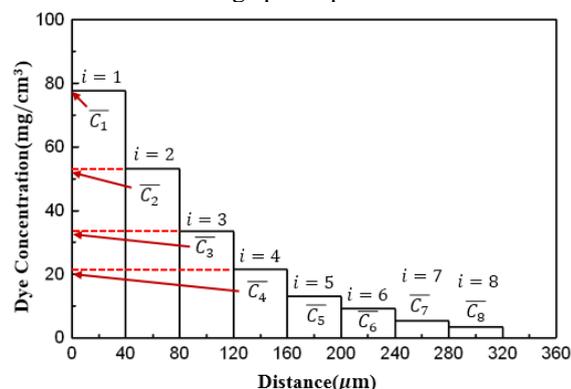


Figure 2. Profile of mean dye concentration (\bar{C}_i) and distance according to the layer number i for the sublimation diffusion by treating at 190°C for 3 hours

Figure 2 shows the mean dye concentrations in terms of the diffusion distance according to the layer number i for the sublimation diffusion of disperse dye to PET by treating at 190°C for 3 hours.

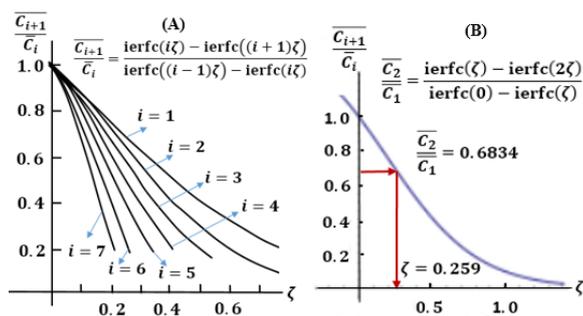


Figure 3. (A) Curves of $\frac{\bar{C}_{i+1}}{\bar{C}_i}$ vs. ζ according to i ; (B) Plot of $\frac{\text{ierfc}(\zeta) - \text{ierfc}(2\zeta)}{\text{ierfc}(0) - \text{ierfc}(\zeta)}$ vs. ζ for $\frac{\bar{C}_2}{\bar{C}_1}$

Figure 3 (A) shows the curves of Eq. (42) according to the layer number i . The ζ value for each layer number i can be determined by the concentration ratio between adjacent layers from the curve for each layer. Figure 3 (B) shows the process of determining the value of ζ for the layer number $i = 1$.

Table 1: Values of $\text{ierfc}(i\zeta)$ according to ζ and i

ζ	i	$\text{ierfc}(i\zeta)$	ζ	i	$\text{ierfc}(i\zeta)$
0.259	0	0.56149	0.156	4	0.14665
	1	0.34262		5	0.09645
	2	0.19115		6	0.06121
0.252	1	0.34764	0.188	5	0.06047
	2	0.19773		6	0.03324
	3	0.10311		7	0.01738
0.216	2	0.23432	0.162	6	0.05482
	3	0.13781		7	0.03258
	4	0.07585		8	0.01858
0.210	3	0.14440			
	4	0.08132			
	5	0.04289			

Table 1 presents the values of $\text{ierfc}(i\zeta)$ according to the values of ζ and the layer number [19]. When the value of ζ was 0.259, the value of Eq. (42) was closest to \bar{C}_2/\bar{C}_1 . The validity of $\zeta=0.259$ for \bar{C}_2/\bar{C}_1 was verified by calculating Eq. (42). The diffusion coefficient between adjacent layers can be calculated by $\zeta = \varepsilon/\sqrt{4Dt}$. The diffusion coefficient between the first layer and the second layer calculated by putting $\zeta=0.259$ into Eq. (43) was $3.313 \times 10^{-7} \text{ cm}^2 \cdot \text{min}^{-1}$.

$$D = \frac{\varepsilon^2}{4t\zeta^2} = \frac{(4 \times 10^{-3})^2}{4 \times 180 \times 0.259^2} \approx 3.313 \times 10^{-7} \left(\frac{\text{cm}^2}{\text{min}} \right) \quad (43)$$

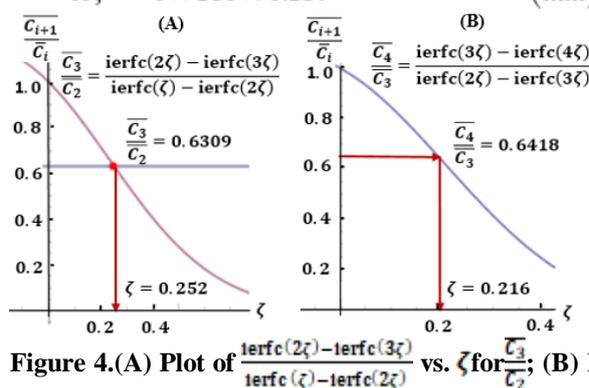


Figure 4. (A) Plot of $\frac{\text{ierfc}(2\zeta) - \text{ierfc}(3\zeta)}{\text{ierfc}(\zeta) - \text{ierfc}(2\zeta)}$ vs. ζ for $\frac{\bar{C}_3}{\bar{C}_2}$; (B) Plot of $\frac{\text{ierfc}(3\zeta) - \text{ierfc}(4\zeta)}{\text{ierfc}(2\zeta) - \text{ierfc}(3\zeta)}$ vs. ζ for $\frac{\bar{C}_4}{\bar{C}_3}$

Figure 4 (A) shows the process of determining the value of ζ for the layer number $i=2$, and Figure 5 (B) also shows the process of determining the value of ζ for the layer number $i=3$. When the value of ζ was 0.252, the value of Eq. (42) was closest to \bar{C}_3/\bar{C}_2 , and when the value of ζ was 0.216, the value of Eq. (42) was closest to \bar{C}_4/\bar{C}_3 .



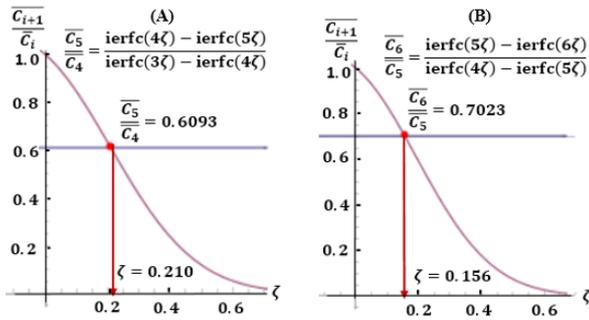


Figure 5.(A) Plot of $\frac{ierfc(4\zeta) - ierfc(5\zeta)}{ierfc(3\zeta) - ierfc(4\zeta)}$ vs. ζ for $\frac{\bar{C}_5}{\bar{C}_4}$; (B) Plot of $\frac{ierfc(5\zeta) - ierfc(6\zeta)}{ierfc(4\zeta) - ierfc(5\zeta)}$ vs. ζ for $\frac{\bar{C}_6}{\bar{C}_5}$

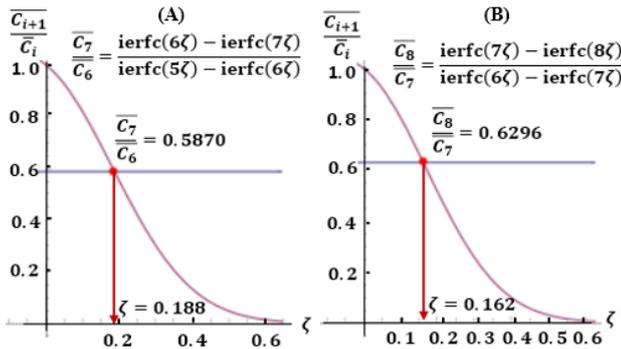


Figure 6.(A) Plot of $\frac{ierfc(6\zeta) - ierfc(7\zeta)}{ierfc(5\zeta) - ierfc(6\zeta)}$ vs. ζ for $\frac{\bar{C}_7}{\bar{C}_6}$; (B) Plot of $\frac{ierfc(7\zeta) - ierfc(8\zeta)}{ierfc(6\zeta) - ierfc(7\zeta)}$ vs. ζ for $\frac{\bar{C}_8}{\bar{C}_7}$

Table 2: Diffusion coefficient between adjacent layers

i	$\frac{\bar{C}_{i+1}}{\bar{C}_i}$	ζ	$\frac{ierfc(i\zeta) - ierfc[(i+1)\zeta]}{ierfc[(i-1)\zeta] - ierfc(i\zeta)}$	D ($\text{cm}^2 \cdot \text{min}^{-1}$)
1	0.6834	0.259	0.6836	3.313×10^{-7}
2	0.6309	0.252	0.6312	3.499×10^{-7}
3	0.6418	0.216	0.6420	4.763×10^{-7}
4	0.6093	0.210	0.6092	5.039×10^{-7}
5	0.7023	0.156	0.7020	9.131×10^{-7}
6	0.5870	0.188	0.5861	6.287×10^{-7}
7	0.6296	0.162	0.6295	8.468×10^{-7}

Figure 5 (A) shows the process of determining the value of ζ for $i=4$, and (B) shows the process of determining the value of ζ for $i=5$. The ζ value obtained from the plot and \bar{C}_5/\bar{C}_4 was 0.210, and that for \bar{C}_6/\bar{C}_5 was 0.156. Figure 6 (A) and (B) also show the process of determining the values of ζ for $i=6$ and $i=7$. The ζ value for \bar{C}_7/\bar{C}_6 was 0.188 and that for \bar{C}_8/\bar{C}_7 was 0.162. The validity of ζ values derived from the ratio of \bar{C}_{i+1} to \bar{C}_i and the diffusion coefficients calculated by $\zeta = \varepsilon/\sqrt{4Dt}$ were presented in Table 2.

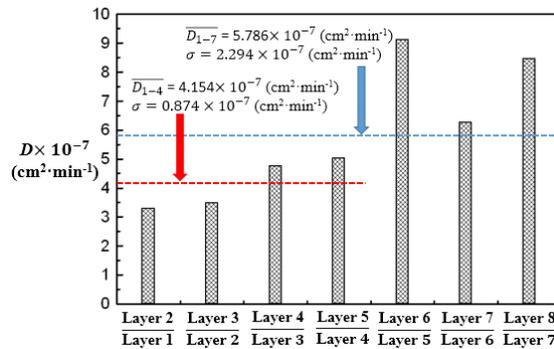


Figure 7. Diffusion coefficients between adjacent layers and the mean diffusion coefficient for the sublimation diffusion of disperse dye by treating at 190°C for 3 hours

Figure 7 shows the distribution of the diffusion coefficients between adjacent layers and the mean diffusion coefficient for the sublimation diffusion of disperse dye by treating at 190°C for 3 hours. The diffusion coefficients for above the 5-th layer were relatively large compared with those for the layers from $i = 1$ to $i = 4$. The mean diffusion coefficient for all the layers (\bar{D}_{1-7}) was $5.786 \times 10^{-7} \text{cm}^2 \cdot \text{min}^{-1}$ and its standard deviation was very large. While the mean diffusion coefficient for the layers from $i = 1$ to $i = 4$ (\bar{D}_{1-4}) was $4.154 \times 10^{-7} \text{cm}^2 \cdot \text{min}^{-1}$ and its standard deviation was small, which was estimated to be appropriate.

3.5. Surface concentration

The surface concentration C_0 can be calculated by the values in Table 1 obtained by putting the determined ζ value into the terms of $ierfc[(i-1)\zeta]$ and $ierfc(i\zeta)$ in Eq. (40). The value of $\frac{1}{\zeta} \{ierfc[(i-1)\zeta] - ierfc(i\zeta)\}$ must be derived from the ζ value and the curves to obtain the ratio of \bar{C}_i to C_0 . Then C_0 is calculated by the known \bar{C}_i .

Table 3: C_0 obtained from \bar{C}_i/C_0 using Eq. (40)

i	\bar{C}_i	$\zeta \left(= \frac{\varepsilon}{\sqrt{4Dt}} \right)$	$\frac{\bar{C}_i}{C_0}$	C_0 ($\text{mg} \cdot \text{cm}^{-3}$)
1	77.7	0.259	0.8555	90.8
2	53.1	0.259	0.5848	90.8
3	33.5	0.252	0.3755	89.2
4	21.5	0.216	0.2869	74.9
5	13.1	0.210	0.1830	71.6
6	9.2	0.156	0.2259	40.7
7	5.4	0.188	0.0849	63.6
8	3.4	0.162	0.0864	39.4



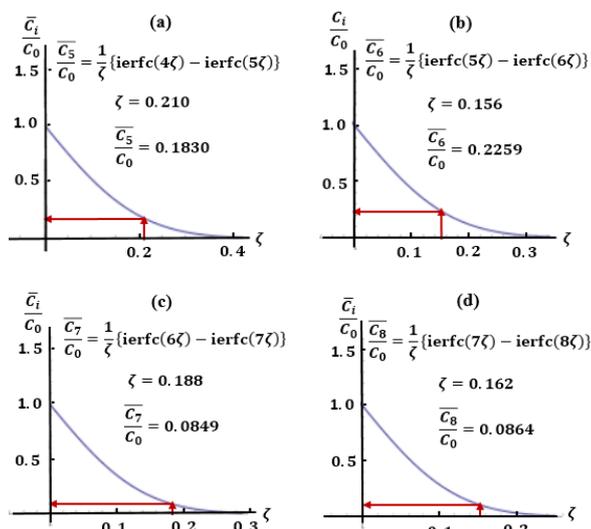


Figure 8. Plots of $\frac{1}{5} \{ierfc[(i-1)\zeta] - ierfc(i\zeta)\}$ vs. ζ and the values of \bar{C}_i/C_0 for $i = 1 \sim 4$

Figure 8 shows the process of determining the ratio of \bar{C}_i to C_0 by the ζ value for the layer number i , where (a) is for $i = 1$, (b) is for $i = 2$, (c) is for $i = 3$, and (d) is for $i = 4$. The ratio of \bar{C}_i to C_0 by the ζ value for $i = 5 \sim 8$ are determined in the same process. The surface concentrations derived by the ratios of \bar{C}_i to C_0 and the ζ values for each layer were presented in Table 3. The surface concentrations derived from the layers above $i = 4$ were unsuitable because they were below the mean dye concentration of the first layer. But the surface concentration derived from the layer of $i = 3$ was suitable.

IV. CONCLUSION

The Laplace transform were applied to finding the solution of the diffusion equation for the diffusion in a semi-infinite medium. The process to calculate the diffusion coefficient using the iterated complementary error function was proposed. For the sublimation diffusion of disperse dye to PET by treating at 190°C for 3 hours using a film roll method, the mean dye concentration in i -th layer was determined using spectrophotometer, and the diffusion coefficient was calculated by obtaining the variable value of the iterated complementary error function from the ratio of the mean dye concentrations between adjacent layers. The mean diffusion coefficient and its standard deviation were also discussed. The surface concentration was calculated by putting the ζ value into the equation of the iterated complementary error function and discussed.

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