

# Performance of Zinc Coated Electrode Wire and Parametric Optimization During Profile Cutting of Die-Steel



M. Saravanan, C. Thiagarajan, S. Somasundaram

**Abstract:** In this work, the effect of brass wire coated with zinc as electrode wire towards maximizing MRR and minimizing SR for the considered input parameters was studied in elaborate during profile cutting of tool steel AISI D3. Experiments were designed based on the  $L_{18}(2^1, 3^7)$  Taguchi's orthogonal array considering cutting speed, Ton and Toff, wire tension, servo feed rate and voltage, current and electrode feed rate. The outputs MRR and SR were analyzed and optimized using Grey Relational Analysis (GRA) simultaneously. For both SR and MRR, the drawn chart shows that, the raw data's lies within upper and lower control limits. The optimum input conditions obtained for higher MRR and lower SR were: 75% of cutting speed, 128  $\mu$ sec of Ton, 54 $\mu$ sec of Toff, 190A of input current, electrode feed of 3 mm/min with 7 gm of electrode tension, 10V of servo voltage and 2060 mm/min of 10V. Execution of ANOVA on grey grade identifies that, wire tension was the parameter that influences more by 25.89%, followed by Ton and servo voltage by 21.37% and feed rate of wire by 11.89%, with an R2 value of 96.55%. For validating the results, confirmation experiment was also done.

**Keywords:** WEDM, Grey Relational Analysis, Taguchi's DoE, Profile Cutting, ANOVA.

## I. INTRODUCTION

Wirecut- Electrical Discharge Machining (WEDM) is advancement of EDM, is a process of metal removing that utilizes thermal energy and uses an uninterruptedly moving electrode wire to eradicate material by means of controlled, rapid and discharges of repetitive sparks. For flushing the particles removed, a dielectric fluid is applied, apart from that, it is also used to regulate the spark discharge, and to cool the workpiece and wire electrode. In WEDM, both the workpiece and wire must be conductive to electricity [1].

In WEDM, as illustrated in Fig. 1, a supply reels supplies the electrode wire, which moves through the conductive workpiece and is taken by the take-up reel.

The wire electrode is advanced gradually between the supply and take-up reels in order to compensate towards the wear that occurs in the wire electrode during at the cutting point.

In WEDM, with a series of spark discharges that happen between the workpiece and precisely placed wire that is moving, machining of materials takes place [2]. High frequency pulses are utilized to create discharges from the moving wire electrode towards the workpiece within a spark gap that is very small which is filled with insulated dielectric fluid, i.e., de-ionized water. The heat generated by sparks, erodes away a minute amount of material by melting and vaporization from the workpiece. During the process, some amount of wire electrode material will also be eroded. These debris particles are removed from the zone of machining by flushing action with the aid of de-ionized water stream that flows through the bottom and top flushing nozzles with extreme pressures [3].

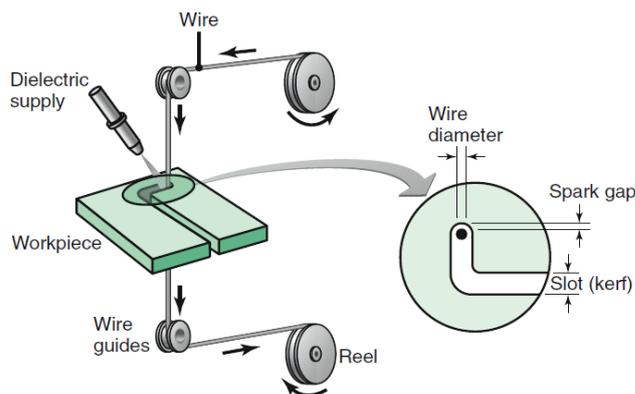


Fig. 1. WEDM process [4]

Tonday and Tigga [5] performed experimental investigation on WEDM while cutting Inconel 718 material considering Ton, Toff, cutting voltage, flushing pressure, and wire feed towards optimizing machining time and surface roughness considering  $L_{27}$  Taguchi's design of orthogonal array (OA) and found that, Ton, is most influential parameter for both outputs and kerf fluctuates with variations in the considered independent parameters during the process of machining. Experimental investigation on MRR and Ra of Inconel 625 were studied in WEDM procedure by adopting tow wire electrodes viz., untreated and cryogenically treated zinc coated wire [6], considering intensity of current,

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tool electrode, Ton, Toff, wire feed rate and tension, a suitable  $L_{18}$  OA was selected, observation shows that, the significant inputs that influences SR and MRR were Ton, wire electrode material and intensity of current. Cryogenic treated zinc coated wire, intensity of current and Ton are the significant inputs that influences the outputs and performance machining improves with cryogenically treated wire electrode.

Kumar et al. [7] analyzed and examined the impact of electrode in WEDM machinability of Inconel 718, considering  $L_{16}$  OA for input parameters Ton, current discharge, flushing pressure and wire speed and studied their influence on corner error and surface roughness. Zinc coated wire electrode provides improved effect on corner radius and SR than the uncoated brass wire. The Ton and discharge current are the highest influential factor that influences the response variables. Kumar et al. [8] conducted experimental studies considering  $L_9$  OA for machining H13 tool steel using WEDM for parametric optimization, considering Ton, Toff and wire tension and speed as inputs and MRR, wire wear ratio and surface flatness as outputs, with zinc coated copper wire electrode. Chinnadurai and Vendan [9] performed WEDM machining using uncoated and zinc coated wire electrode during machining AISI 4140. Observation shows that, MRR was affected by current, Ton for uncoated brass wire, and for coated wire electrode, Ton, servo voltage and Toff are the influential parameters than govern the MRR. The best performances were provided while using wire electrode as zinc coated brass wire.

Kapoor et al. [10] studied the influence of different wire electrodes used in WEDM on the machining characteristics of AISI D3 die steel, considering brass wire, zinc material coated wire and composite wire along with Ton and peak current, over the outputs SR and cutting speed. The study found that, reduction in SR was possible with brass wire and improved cutting speed was possible with composite wire when compared with other wire electrodes. With brass wire, smooth surface is attained, whereas rough surface is produced with zinc coated electrode wire. Dhale and Kulkarni [11] studied the behavior of Inconel-718, with different wire electrodes in WEDM process and measured the performance measures such as MRR and surface finish, conducted experiments by varying Ton, Toff, wire tension, dielectric fluid flushing pressure and wire feed. The investigational output proves that, better MRR and SR was better. Improved MRR is possible with coated wire than uncoated wire, zinc coated wire gives better surface finish as compared to brass wire. Researches had also considered different wire electrodes during WEDM process parameter optimization purpose [12].

From the review of literature carried out, the conclusion was, no researcher had adopted most of the WEDM process parameters for optimization for their study and the works on brass wire coated with zinc is limited. Hence, an attempt was made to perform the WEDM studies using zinc coated wire electrode. In this work, the influence of wire electrode coated with zinc along with the effect of machining parameters were studied during the profile cutting of tool steel in WEDM. Experiments were formulated as per Taguchi's methodology

and the outputs measured (MRR and SR) were analyzed using Grey Relational Analysis. The process capability of WEDM was studied using control chart.

## II. MATERIALS & METHODOLOGY

### A. AISI D3 Steel

In this work, AISI D3 high carbon, high chromium steel termed as tool grade was selected as workpiece. D3 steels were characterized with extreme hardness through oil hardening and due to the presence of carbides of chromium in their microstructure [13]. The elements present in AISI D3 steel is presented in Table I. D3 tool steels are specifically used as tooling and cold die materials and in trimming and blanking dies. A commercially available zinc coated brass wire is preferred as electrode with a diameter of 0.25 mm diameter. For experimentation purpose a plate of size 50×50×15 mm was used.

Table- I: AISI D3 steel composition

Element	C	Si	Mn	P	S	Cr	Fe
%	2.	0.60	0.60	0.030	0.032	11.9	Reminder
	4	8	1	3	2	6	

### B. Taguchi's Experimental Methodology

The method of examining and describing all possible situations in an experimental trial that comprises of various design parameters is known as Design of Experiments (DoE) [14]. Taguchi believed that the perfect practice to augment the quality of a product is to develop the product with inbuilt quality [15]-[17]. For achieving this quality, Taguchi planned investigational methods using specifically created arrays known as Orthogonal Arrays (OA) [18], [19]. Experimental design was made easier and consistent with the use of table designed using OAs. Taguchi established distinct OAs for his investigation that are purely constructed on Latin squares, with combination of considered input is a specific means, for various experimental trials [20]. Enhancing the design of a product suggests that finding the exact combination of input parameters or developing appropriate modifications to the machinery will provide better outcomes. Experiments designed based on OA reduces the variation in outputs due to properly controlled parameters.

For examining the machinability performance of D3 steel, a  $L_{18}$  OA was selected for multiple-level input factors [21] for dissimilar number of levels of input parameters for conducting trials, with the aid of Minitab-18 a statistical analysis software in which one parameter varies through two level and other selected parameters were varied by three level values. From Taguchi's OA for multi-level model, the various combination of input parameter selected for machining designed as per Latin square is given in Table II.



Table- II: Taguchi L<sub>18</sub> OA

Trial No	Cutting Speed (%)	Ton (μsec)	Toff (μsec)	Input Current (Amp)	Wire Feed (mm/min)	Wire Tension (gm)	Servo Volt (Voltage)	Servo Feed rate (mm/min)
1	70	126	48	190	3	7	10	2060
2	70	126	51	210	4	9	15	2080
3	70	126	54	230	5	11	20	2100
4	70	127	48	190	4	9	20	2100
5	70	127	51	210	5	11	10	2060
6	70	127	54	230	3	7	15	2080
7	70	128	48	210	3	11	15	2100
8	70	128	51	230	4	7	20	2060
9	70	128	54	190	5	9	10	2080
10	75	126	48	230	5	9	15	2060
11	75	126	51	190	3	11	20	2080
12	75	126	54	210	4	7	10	2100
13	75	127	48	210	5	7	20	2080
14	75	127	51	230	3	9	10	2100
15	75	127	54	190	4	11	15	2060
16	75	128	48	230	4	11	10	2080
17	75	128	51	190	5	7	15	2100
18	75	128	54	210	3	9	20	2060

C. Multi-Criteria Optimization Method

Grey Relational Analysis (GRA) is implemented for perceiving the ideal assemblage of input factors for attaining improved responses [22]-[24]. GRA is applied for assessing the dependent parameter influence with meager data information [25]. In grey approach, pre-processing of raw data's is made initially for further analysis, pre-processing is done by converting the data points to some type of indices for quantification purposes through normalizing procedure [26]. The experimental output values should be converted to decimal values between zero and one for assessing in normalizing stage [27]. In normalizing, for larger-the-better condition, the original raw data should be converted using the formulae;

$$x_i^*(k) = \frac{x_i^0(k) - \min x_i^0(k)}{\max x_i^0(k) - \min x_i^0(k)} \quad (1)$$

where  $x_i^0(k)$  is raw data,  $x_i^*(k)$  corresponds to data subsequent to normalization,  $\max x_i^0(k)$  is higher value of data and  $\min x_i^0(k)$  is the lower data value. For performing normalizing responses that falls under lower-the-better category, the general formulae used is:

$$x_i^*(k) = \frac{\max x_i^0(k) - x_i^0(k)}{\max x_i^0(k) - \min x_i^0(k)} \quad (2)$$

Following normalizing, determination of grey coefficient is carried out for determining the relationship that exists between ideal and real values of normalization [28], the formulae used for finding grey coefficient is,

$$\zeta_i(k) = \frac{\Delta_{\min} + \zeta \cdot \Delta_{\max}}{\Delta_{0i}(k) + \zeta \cdot \Delta_{\max}} \quad (3)$$

$\Delta_{0i}(k)$  is deviation of normalized values for the ideal value of one, taken as reference value, provided as,

$$\Delta_{0i}(k) = \left\| x_0^*(k) - x_i^*(k) \right\| \quad (4)$$

$$\Delta_{\max} = \max_{\forall j \in i} \max_{\forall k} \left\| x_0^*(k) - x_j^*(k) \right\|, \quad (5)$$

$$\Delta_{\min} = \min_{\forall j \in i} \min_{\forall k} \left\| x_0^*(k) - x_j^*(k) \right\|$$

$\zeta$  is identification coefficient, usually  $\zeta \in$  lies in the range of 0 to 1 and normally  $\zeta$  is considered as 0.5. After calculating grey coefficient value, the corresponding grade values were determined by considering the mean values of grey coefficient equivalent to experimental trials as,

$$\gamma_i = \frac{1}{n} \sum_{k=1}^n \zeta_i(k) \quad (6)$$

D. Experimental Setup

Experiments were performed on computer-controlled Electronica ELCUT WEDM machine as per the formulated L<sub>18</sub> OA and each experiment was replicated thrice for finding reliable outputs. After carrying out the machining, SR measurement was performed on surface of specimens with the help of Surfcoorder SE1200 with specifications: 520 μm and 25 mm measuring range in vertical and horizontal directions with 0.008 μm resolution and 0.8 mm cut-off with gaussian type filter. Through loss of volume, MRR was calculated with the consideration of machining time. MRR is calculated using the formulae;

$$MRR = \frac{Wt. \text{ before } m/c - Wt. \text{ after } m/c}{M/c \text{ time} \times \text{Density}} \text{ (mm}^3/\text{min)} \quad (7)$$

III. RESULT AND DISCUSSIONS

As per L<sub>18</sub> Taguchi's design, experiments were conducted, and the MRR and SR was determined from the volume loss and roughness on the machined surface, as presented in Table III. Observation shows that, with higher cutting speed, both MRR and SR increases [29]. With increase in Ton, MRR increases considerably, but SR increases up to 127 μsec and with further increase in Ton to 128 μsec, SR reduces. With higher Toff, MRR increases abruptly [30] but SR increases up to 51 μsec, afterward SR decreases. Similarly, with higher input current, MRR increases but SR increases initially and afterwards it reduces considerably.



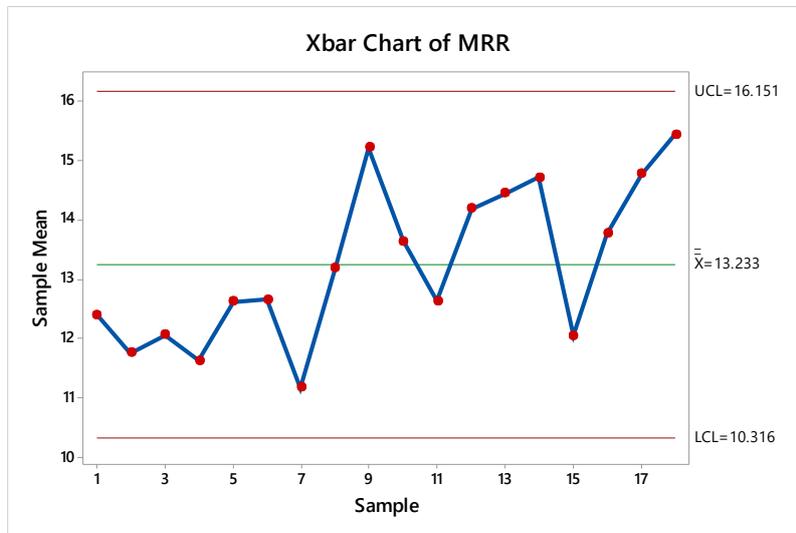
With higher wire feed, SR increases drastically [31], but MRR reduces until 4 mm/min and then upsurges with higher feed rate of wire electrode.

**Table- III: Output response of WEDM with zinc coated wire**

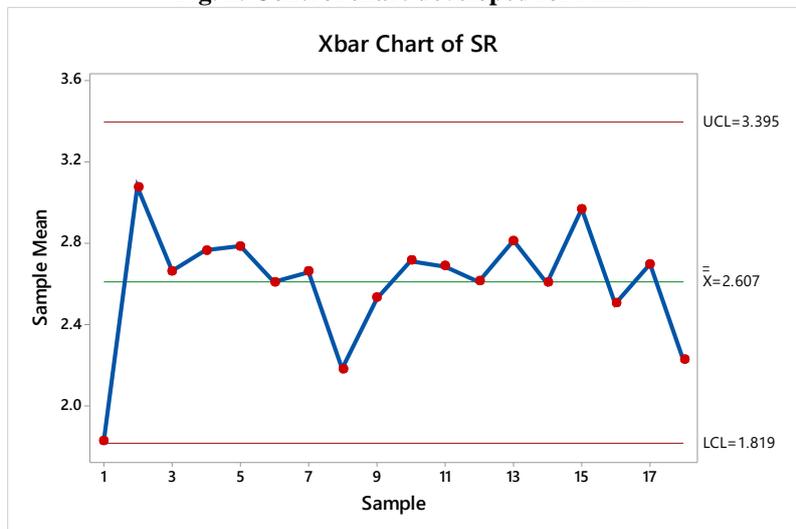
Exp. No	Output Responses	
	MRR (mm <sup>3</sup> /min)	SR (μm)
1	12.390	1.827
2	11.745	3.076
3	12.048	2.664
4	11.619	2.763
5	12.619	2.786
6	12.649	2.607
7	11.169	2.660
8	13.169	2.181
9	15.212	2.531
10	13.636	2.715
11	12.623	2.687
12	14.182	2.611
13	14.442	2.811
14	14.701	2.604
15	12.039	2.969
16	13.762	2.503
17	14.762	2.698
18	15.429	2.226

With higher wire tension, SR increases significantly, but MRR tends to reduce. SR become higher with higher values of servo voltage to 15 V, afterwards SR decreases, whereas for MRR, initially MRR decreases until 15 V, then it tends to increase with higher servo voltage to 20 V. With higher servo feed, SR tends to increase, but MRR increases with change in servo feed rate up to 2080 mm/min, with further increase to 2100 mm/min, MRR tends to reduce.

For assessing the process control and stability, the statistical tool normally used is X-bar chart [32], which can identify, whether the process is foreseeable and steady [33]. Fig. 2 shows the control chart (X-bar) for MRR, where the upper limit is 16.151 mm<sup>3</sup>/min and lower limit is 10.316 mm<sup>3</sup>/min. It was observed that, all the experimental data points were well scattered within the control limits, thereby the stable experimental readings were evaluated. Likewise, control chart obtained for SR is presented in Fig. 3, having higher control limit of 3.395 microns and lower control limit of 1.819 microns, all the 18-trial data were placed well within control limits.



**Fig. 2. Control chart developed for MRR**



**Fig. 3. Control chart developed for SR values**

For optimizing SR and MRR simultaneously, GRA was applied, for normalizing raw data's of MRR and SR which should be maximum and minimum, for which formulae given in Equ. (1) and Equ. (2) were used. Following the normalizing

sequence, deviation sequence was calculated, to know how much the normalized values had deviated from the ideal value of 1, as displayed in Table IV.

**Table- IV: Normalizing and Deviation sequence in GRA**

Trial No	Normalizing Sequence		Deviation Sequence		Grey Relational Coefficient		Grey Relational Grade
	MRR	SR	MRR	SR	MRR	SR	
1	0.287	1.000	0.713	0.000	0.412	1.000	0.706
2	0.135	0.000	0.865	1.000	0.366	0.333	0.350
3	0.206	0.330	0.794	0.670	0.386	0.427	0.407
4	0.106	0.251	0.894	0.749	0.359	0.400	0.379
5	0.340	0.232	0.660	0.768	0.431	0.394	0.413
6	0.347	0.376	0.653	0.624	0.434	0.445	0.439
7	0.000	0.333	1.000	0.667	0.333	0.428	0.381
8	0.469	0.717	0.531	0.283	0.485	0.638	0.562
9	0.949	0.436	0.051	0.564	0.908	0.470	0.689
10	0.579	0.289	0.421	0.711	0.543	0.413	0.478
11	0.341	0.311	0.659	0.689	0.432	0.421	0.426
12	0.707	0.372	0.293	0.628	0.631	0.443	0.537
13	0.768	0.212	0.232	0.788	0.683	0.388	0.536
14	0.829	0.378	0.171	0.622	0.745	0.446	0.595
15	0.204	0.086	0.796	0.914	0.386	0.354	0.370
16	0.609	0.459	0.391	0.541	0.561	0.480	0.521
17	0.843	0.303	0.157	0.697	0.762	0.418	0.590
18	1.000	0.681	0.000	0.319	1.000	0.610	0.805

Table IV presents the grey coefficient values obtained from the deviation sequence as given in Equ. (3). By taking mean grey coefficient values, corresponding to independent level values of input factors, GRGs were obtained and it was noticed that, for the experimental trial 18, higher value of GRG was obtained. For plotting the GRG response plot, mean grey grade that corresponds to individual level values were taken as presented in Fig. 4, based on the calculation of response table as in Table V. Optimum level values evolved from response table and response plot were selected based on higher values of grey relational grade, optimum settings identified were: 75% of cutting speed, 128 μsec of Ton, 54μsec of Toff, 190 A of input current, 3 mm/min of wire feed rate, 7 gm of tension of wire electrode, 260 mm/min and 10V of servo feed rate and voltage.

Interaction graph drawn for the obtained GRG to study the combinatory influence one parameter over another parameter

[34] is given in Fig. 5. Observation shows that, in between cutting speed and input current, cutting speed and wire tension, a significant interaction exists, represented by non-parallel lines. In between T<sub>on</sub> and wire tension, input current, servo feed and T<sub>off</sub> a considerable interaction was observed. A combined effect between T<sub>off</sub> and electrode tension and current and T<sub>off</sub> and servo feed was observed through non-parallel lines. In between input current and feed rate of wire electrode a considerable interaction effect was observed, but with other input parameters no significant effect was observed. Among wire feed and tension, feed rate of the wire electrode and servo voltage and between wire feed and servo feed a significant interaction exists. Combined effect of wire tension and servo feed and between servo voltage and servo feed was higher.

**Table- V: Mean level values of GRG**

Factors	Level 1	Level 2	Level 3	Max - Min
Cutting Speed	0.481	0.540	-	0.059
Ton	0.484	0.455	0.591	0.136
Toff	0.500	0.489	0.541	0.052
Input Current	0.527	0.504	0.500	0.026
Wire Feed	0.559	0.453	0.519	0.106
Wire Tension	0.562	0.549	0.419	0.142
Servo Volt	0.577	0.435	0.519	0.142
Servo Feed rate	0.556	0.493	0.482	0.074

A statistical approach for evaluating the amount of variation between sets of data is Analysis of Variance (ANOVA), which is a needful tool identified by researchers for evaluating the dependent variables based on the influence of independent variables [35]. From the statistical tool ANOVA executed on GRG, it was identified that, wire tension was the most influential parameters contributing by 25.89%, followed by

Ton and servo voltage by 21.37% and feed rate of wire by 11.89%. With 95% confidence level of ANOVA, an error of 3.45% was obtained, thereby producing a better model as displayed in Table VI. The R<sup>2</sup> value of the developed model is 96.55%, which is a good one. The influence of different independent parameters on grey grade determined is presented in Fig. 6.



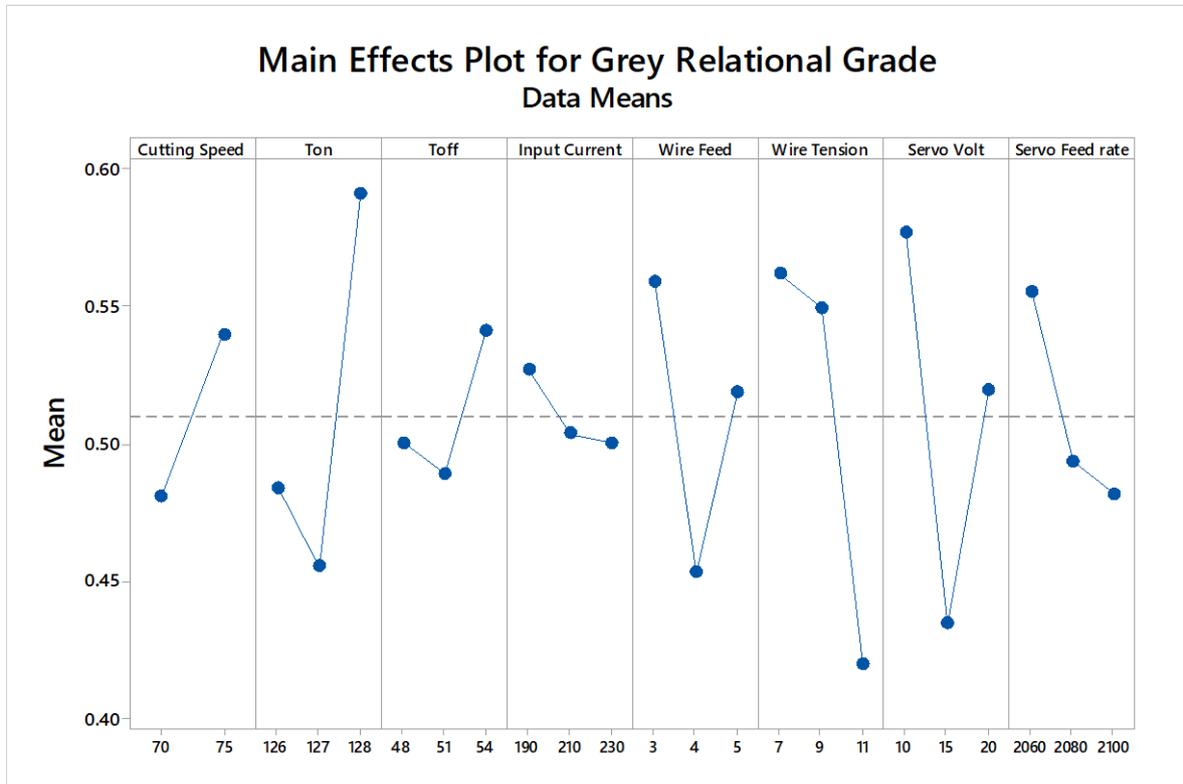


Fig. 4. Main effect plot for GRA Grade

Table- VI: ANOVA for Grey relational grade

Source	DoF	Adj. SS	Adj. MS	F Value	P Value	% Contribution
Cutting Speed	1	0.0157	0.0157	3.169	0.217	5.46%
Pulse ON-Time	2	0.0614	0.0307	6.200	0.139	21.37%
Pulse OFF-Time	2	0.0090	0.0045	0.907	0.524	3.13%
Input Current	2	0.0025	0.0012	0.249	0.801	0.86%
Wire Feed rate	2	0.0342	0.0171	3.451	0.225	11.89%
Wire Tension	2	0.0744	0.0372	7.511	0.117	25.89%
Servo Voltage	2	0.0614	0.0307	6.201	0.139	21.37%
Servo Feed rate	2	0.0190	0.0095	1.913	0.343	6.59%
Error	2	0.0099	0.0050	1.000		3.45%
Total	17	0.2875	0.0169			100.00%

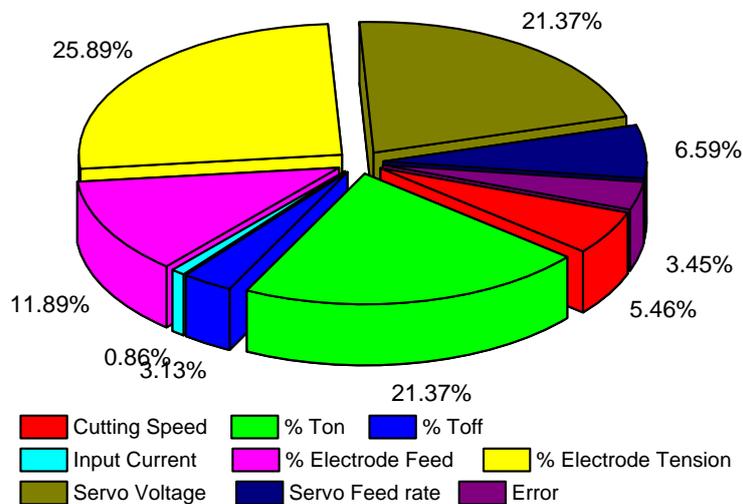


Fig. 6. Contribution of dependent parameters on GRG

### Interaction Plot for Grey Relational Grade Data Means

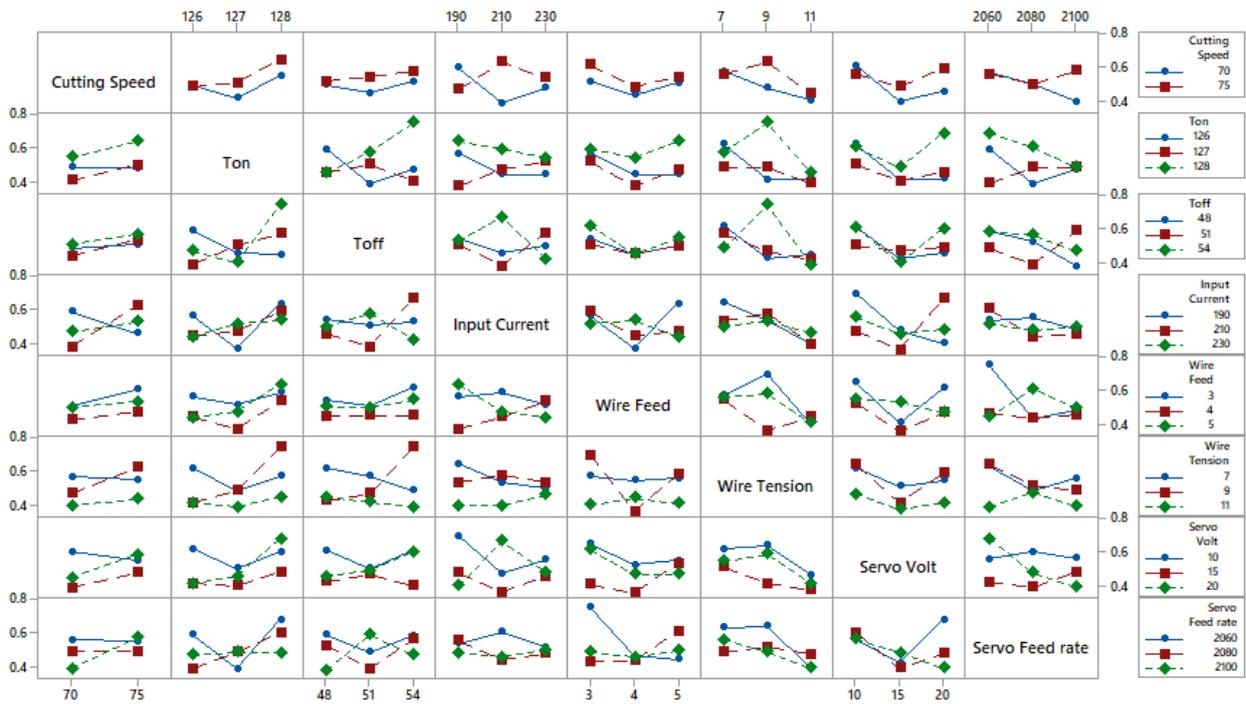


Fig. 5. Interaction plot for GRG

Surface plots are figures of 3D in nature, relatively displaying the data points of individuals, these plots of surface present a functional association that exists among the selected dependent variable (Y), and two input independent variables such as X and Z [36]. The 3D response plot is an alternative and identical design to the contour plot. A response surface is a geometric illustration attained once an output parameter is designed as a relationship with one or more quantitative independent factors [37]. Response surface plots were drawn for the output responses SR and removal of material from workpiece for the most significant parameters based on the ANOVA table. Fig. 7 shows the surface plot drawn between

Ton and wire feed and between Ton and wire tension for variation in MRR. Observation shows that, with increase in Ton, MRR tends to shoots up in a linear manner and with higher values of tension in wire electrode, MRR tends to reduce in a curvilinear condition, similarly with higher wire feed rate, MRR tends to increase in a non-linear way. Higher Ton and feed rate of wire electrode produce lower MRR, whereas higher Ton and lower wire tension produces a higher MRR.

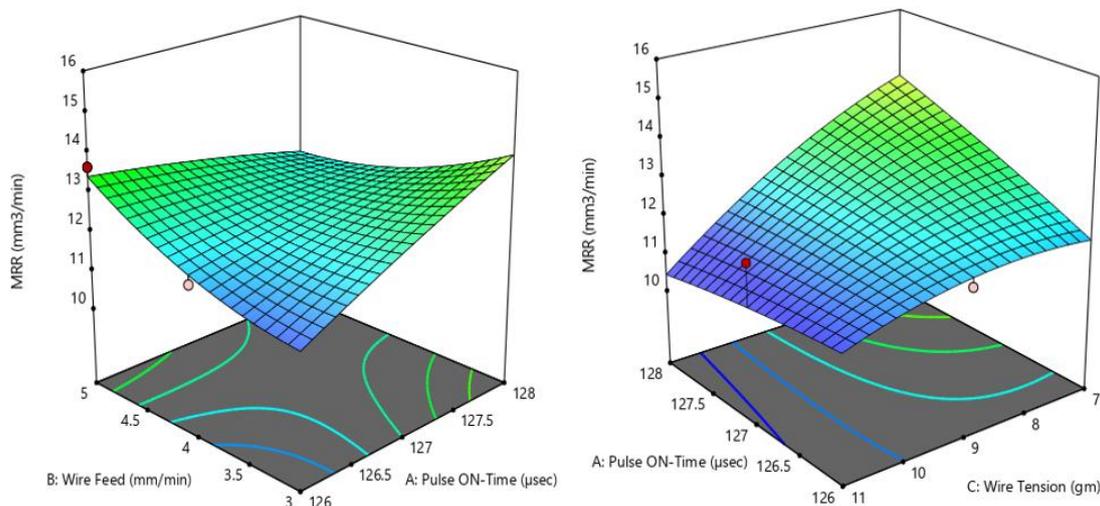


Fig. 7. Surface plot for MRR over wire tension, Ton and wire feed

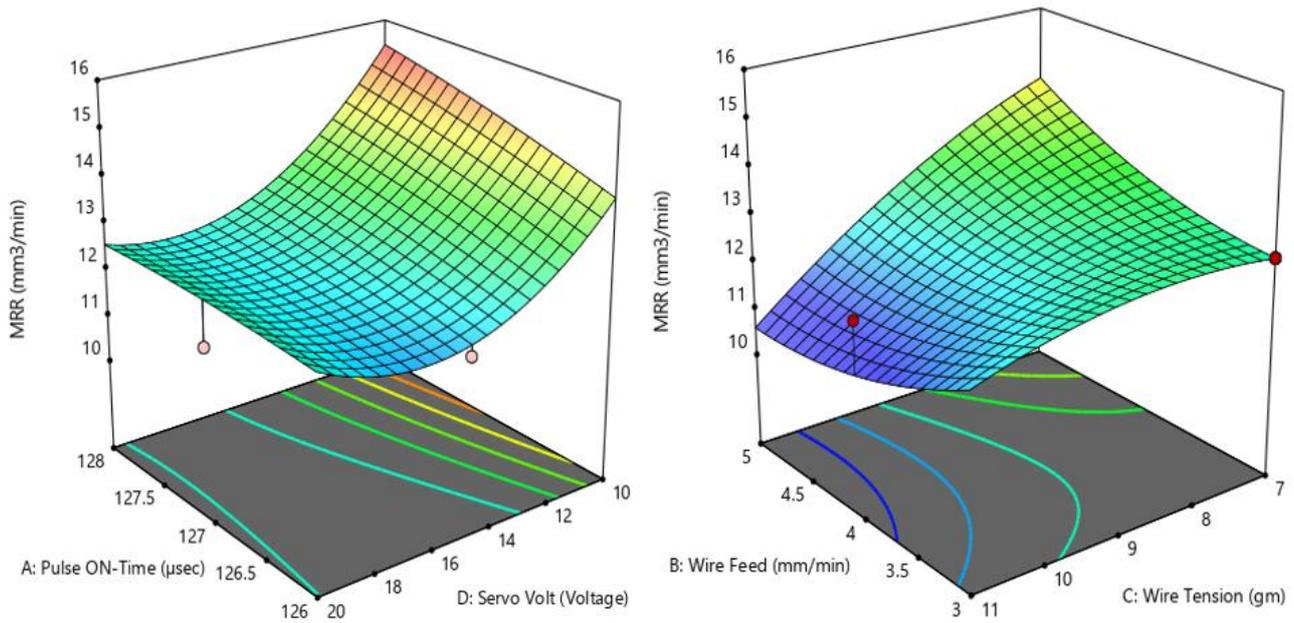


Fig. 8. Surface plot for MRR over Ton, wire feed and tension and servo voltage

Fig. 8 presents the 3D plot for MRR between Ton and servo voltage and between tension in wire and feed rate of wire. With increase in servo voltage, MRR tends to reduce in a concave manner, with a non-linear relationship. Higher Ton and servo voltage produce a higher MRR, and similarly higher MRR was developed for lower wire tension and higher feed rate of wire. Effect of electrode feed rate and servo

voltage, and between servo voltage and tension in wire electrode towards MRR is presented in Fig. 9. Observation made was, maximum MRR was achieved with lower servo voltage values and extreme feed rate of wire electrode. With lower wire tension and lower servo voltage, higher values of MRR was achieved.

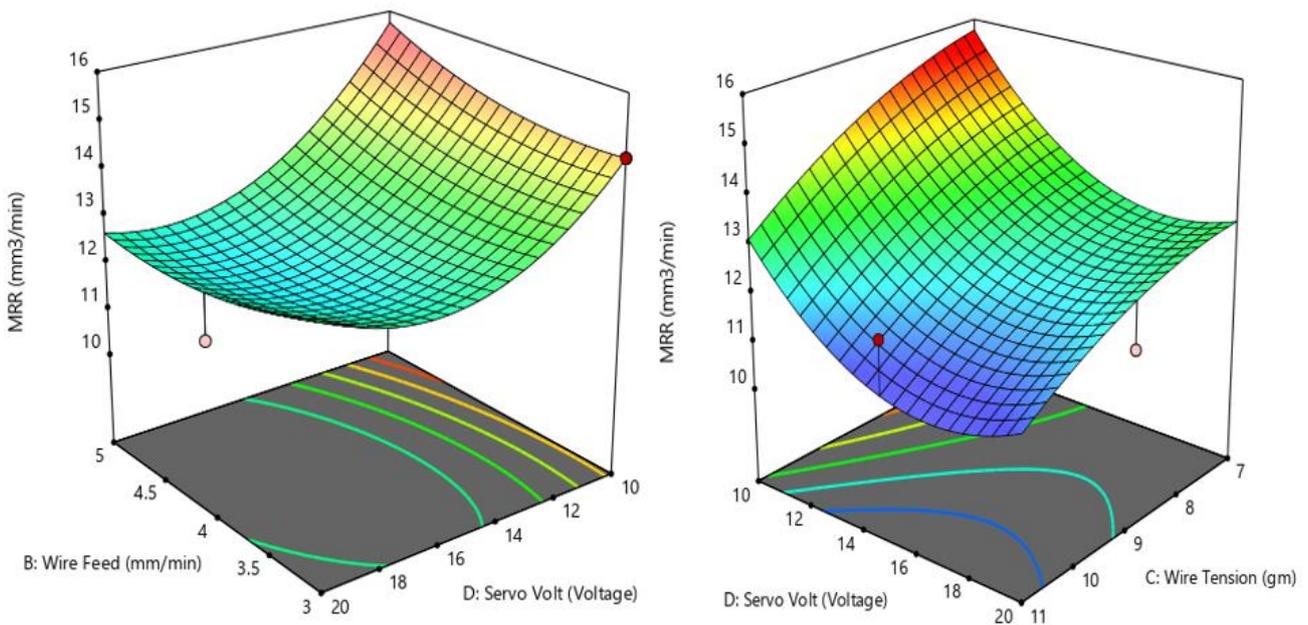
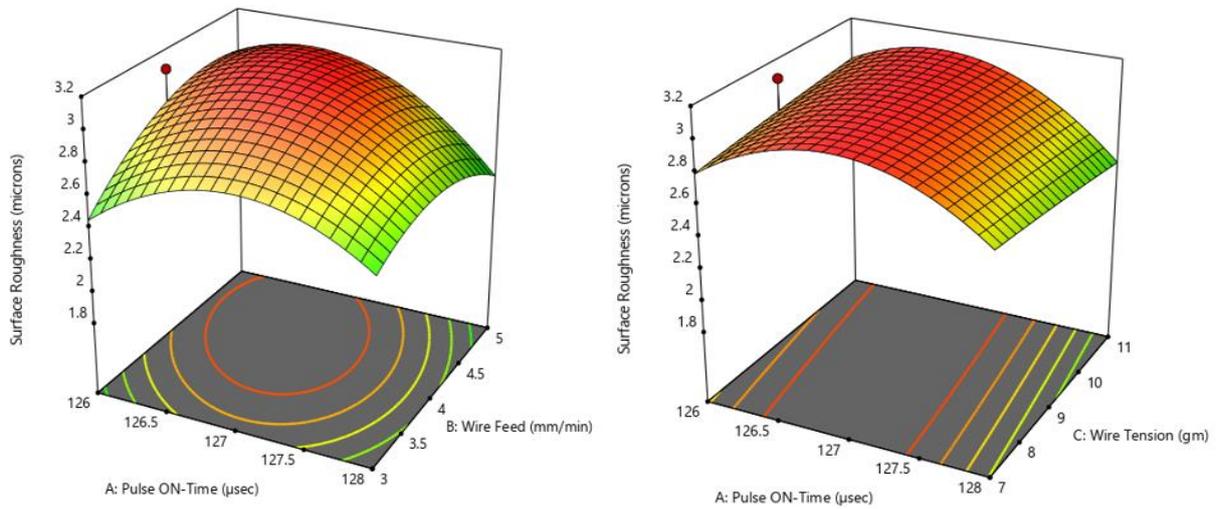


Fig. 9. Surface plot of MRR for servo volt, wire tension and feed rate

A min-max condition was achieved with Ton and feed rate of wire for surface roughness, as presented in Fig. 10. SR increases up to certain value of Ton and wire feed rate, afterwards it tends to reduce. With higher tension in the wire electrode, SR tends to increase. Higher SR was sensed with moderate values of Ton and wire feed rate. For moderate value of Ton and wire tension, higher SR was achieved.

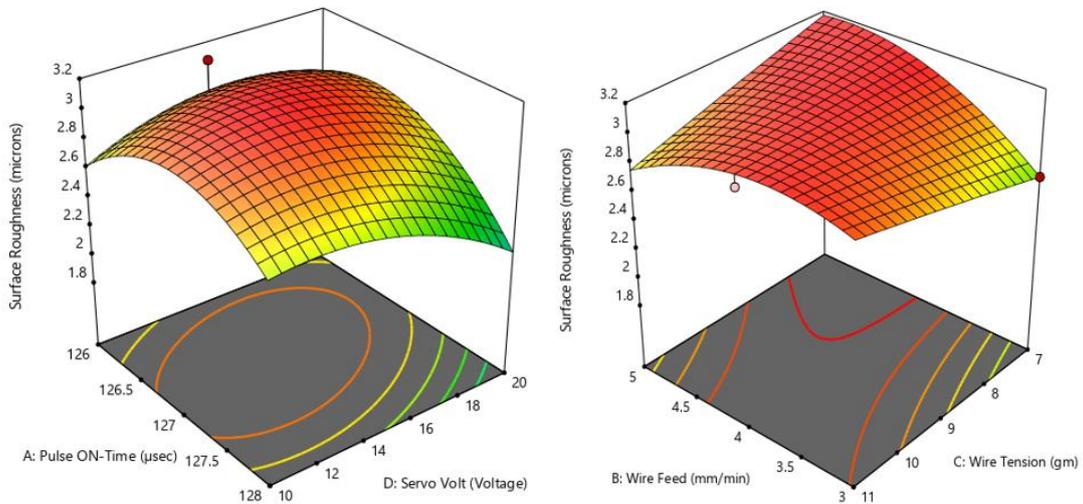
Fig. 11 presents the surface plot for SR for variation in the significant input parameters. With increase in servo voltage, SR tends to reduce in a convex manner. Lower values of servo voltage produce higher SR, along with a moderate value of Ton. Lower tension of wire electrode and higher electrode feed produces a significant increase in SR.



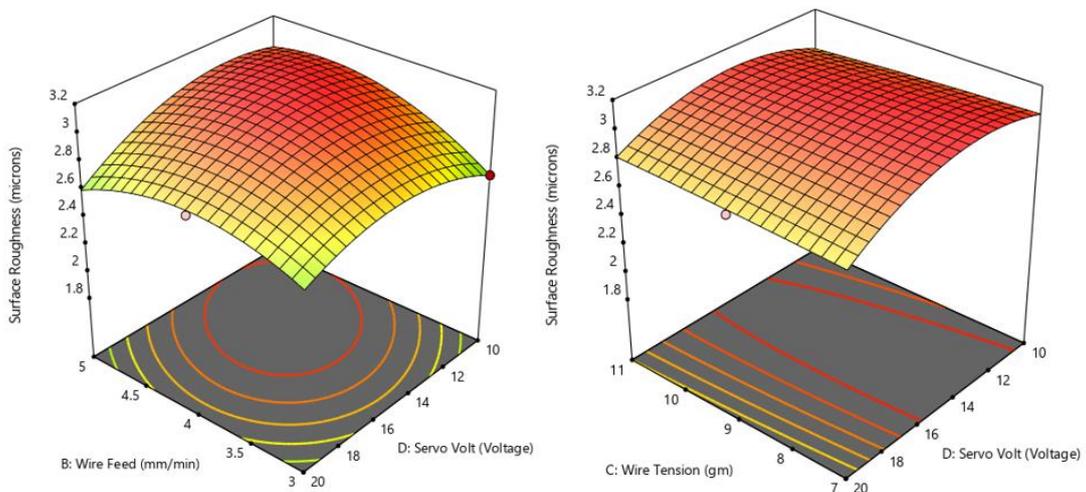
**Fig. 10. Surface plot of SR for wire feed, tension and Toff**

The surface plot of SR for various combinations of servo voltage and wire feed and between servo voltage and tension of wire is presented in Fig. 12. Observation shows that, lower

feed rate of wire and higher-level value of servo voltage produces lower SR, similarly, lower value of wire tension and higher-level value of servo voltage produces a reduced SR.



**Fig. 11. Surface plot of SR for servo volt, pulse-on time, wire tension and wire feed**



**Fig. 12. Surface plot of SR for servo volt, wire tension and wire feed**

**A. Predictive model for Grey Grade**

From the known ideal input factors, the GRG prediction was done for zinc coated wire electrode as given in Equ. (8) [38], [39].

$$\mu_{predicted} = V_{2m} + Ton_{3m} + Toff_{3m} + I_{1m} + WF_{1m} + WT_{1m} + SV_{1m} + SF_{1m} - 7\mu_{mean} \tag{8}$$

where,  $V_{2m}$ ,  $Ton_{3m}$ ,  $Toff_{3m}$ ,  $I_{1m}$ ,  $WF_{1m}$ ,  $WT_{1m}$ ,  $SV_{1m}$  and  $SF_{1m}$  and are the mean values of GRG corresponding to optimal individual levels and  $\mu_{mean}$  is the mean value of obtained GRG for all the 18 experiments. At optimal condition, the value of predicted mean ( $\mu_{predicted}$ ) is calculated as 0.883.

**B. Confirmation Experiment**

For confirming the effectiveness of the obtained optimum input parameters level settings, a validation experiment was made with identical investigational state and outputs obtained are tabulated in Table VII. For the obtained outputs MRR and SR, the equivalent GRG was calculated and is compared with the predicted GRG and the error deviation was calculated, as given in Table 7. A variation of 1.13% was obtained between the experimental and predicted GRG, and it was understood that GRA produces a better solution for multi-objective optimization.

**Table- VII: Comparison of obtained GRGs**

Measured outputs	Exp. values	GRG_Experimental	GRG_Predicted	% of Error
MRR (mm <sup>3</sup> /min)	15.189	0.893	0.883	1.13%
SR (microns)	1.906			

**IV. CONCLUSIONS**

Optimizing the output responses during WEDM profile cutting of D3 steel zinc coated electrode wire towards MRR and SR considering  $L_{18}(2^1, 3^7)$  OA was achieved. From investigational examination, the following inferences were made.

- Higher SR and MRR was achieved with higher cutting speeds. With increase in Ton and Toff, MRR increases considerably, but SR increases until the moderate level value, afterwards it tends to reduce. Similarly, with higher input current, MRR increases but SR increases initially and afterwards it reduces considerably. With higher wire feed, SR increases drastically, but MRR reduces initially, afterwards shoots up with additional rise in wire feed rate. Higher wire tension produces lower MRR and higher SR. A max-min situation arises for MRR and SR when servo voltage is changed. Increasing the servo feed rate increases the SR, but MRR increases with change in servo feed rate up to 2080 mm/min.
- Control chart drawn for SR and MRR identifies that, all the data points were scattered between the two control limits values, thereby the steadiness in experimental trials were proved.
- The optimal settings of level values of independent input parameters identified were: 75% of cutting speed, 128 μsec of Ton, 54μsec of Toff, 190 A of input current, 3 mm/min of wire feed rate, 7 gm of tension of wire electrode, 260 mm/min and 10V of servo feed rate and voltage.
- Interaction plot shows that, between cutting speed and input current, cutting speed and wire tension, a significant interaction exists. A higher combinatory effect was observed between pulse on-time and several inputs (Toff, wire tension, input current, servo feed). Among wire feed and current a substantial collaboration effect was detected, but with other input parameters no significant effect was observed. Combined effect of wire tension and servo feed rate and between servo voltage and servo feed rate was higher.
- From ANOVA executed on GRG, it was identified that,

- wire tension was the utmost significant factor contributing by 25.89%, followed by Ton and servo voltage by 21.37% and wire feed rate by 11.89% with an R<sup>2</sup> value of 96.55%.
- From the confirmation experiment it was found that, a variation of 1.13% was achieved between the predicted and experimental GRGs, and it was understood that GRA produces a better solution for multi-objective optimization.

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