

# Frequency Regulation in Multi Area Power System Optimized By Firefly Swarm Hybridization Algorithm

P.Venkatesh, S.Upender Rao, T.Suneel

Liner Quadratic Regulator using load frequency control [3]. Two area two units inter connected power system controlled by PID controller and optimized by DEPSO [4]. AGC interconnected power system controlled by cascaded

[5].Optimized by DE algorithm [6].

Five areas interconnected power system using Firefly algorithm [7]. Interconnected power system and each area attached to PEV using TLBO optimization technique [8].

controller optimization technique is GWO

Automatic generation control of both areas are fixed to DFIG wind turbine controlled by integral controller [9]. Interconnected thermal power system controlled by PIDF controller by TLBO optimization[10]. Active frequency control by PD-PI controller using TLBO algorithm [11]. Single area controlled by PD-PI controller by using GWO [12].

To Minimize the ITAE function in area1, applied 1% step load distribution. Both areas are connected to the DFIG wind turbine. Speed controller of different penetration levels are 5%, 20% and 50% and it is observed that lower wind penetration improves steady state performance. The performance of the PID controller and PD-PI controller is studied for different penetration levels. Lower penetrations are best performance as compared to higher penetration levels

Area1 consists of three reheat turbine units and area2 consists of three non reheat turbine units. Hybridization algorithm is implemented for PID and cascaded PD-PI controllers and to know the optimum values of the controllers. Area participation factors are area1 are a11+a12+a13=1 and area2 are a14+a15+a16=1.Each unit participation factor taken as 0.33.

$$ACE1 = \Delta P_{12} + B_1 \Delta f_1 \tag{1}$$

$$ACE2 = \Delta P_{21} + B_2 \Delta f \tag{2}$$

Where  $\Delta P_{12}$  and  $\Delta P_{21}$  are represents deviation of tie line powers. Two areas connected to wind DFIG. DFIG generate the electrical power in large wind turbine. Wind energy do not participate frequency control because added to doubly fed induction generator is constant output voltage and constant frequency. Two controllers are implemented to thermal power system.

Abstract: Automatic Generation Control of two area multi unit interconnected thermal power system with dynamic participation of Doubly Fed Induction Generator based on the wind turbines. In this work two areas consisting of three unequal turbines both areas are connected to the DFIG based wind turbine, Area 1 consisting of three reheat turbines with Doubly Fed Induction Generator based on wind turbine and area2 consisting of three non reheat turbines with Doubly Fed Induction Generator based on wind turbine and two areas interconnected by tie line. Two different controllers are used, namely PID and cascaded PD-PI controllers. The controllers effectively tuned by hybridization algorithm. 1% step load disturbance is applied in area 1 for analyzing the dynamic performance. The performance of two area multi-unit power system is done in MATLAB/SIMILINK software. The dynamic response of the considered system is compared in terms of undershoots, overshoot and settling times

Keywords: Automatic Genaration Control(AGC); Proportional Integral Derivative(PID) and cascaded PD-PI controllers; Doubly Fed Induction Generator based wind turbine(DFIG).

#### I. INTRODUCTION

Two areas 1 and 2 interconnected by a tie line. The main objectives of AGC are to maintain zero steady state error in frequency deviation and tie line power deviation. There are many control techniques are used to maintain constant frequency. Area1 and area2 are connected by the DFIG with turbine. In this paper wind energy is also considered. Now a day's most of the electrical power is generated using DFIG wind turbines. DFIG is to control the active and reactive power required system operation.

In the literature survey several optimization techniques and control strategies have been proposed in the field of LFC. In LFC of single area thermal power system controlled by the PID and integral controller and optimized by PSO optimization technique [2].

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#### II POWER SYSTEM INVESTIGATED

### A. Power system network used in this work

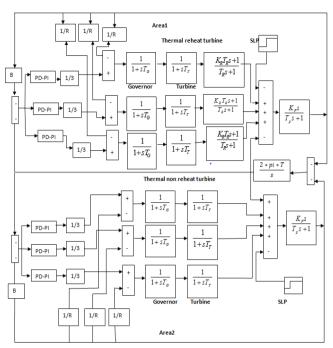


Fig.1 Two area three unit thermal power system

#### **B. Structure of controllers**

PID controllers used in many control applications.PID controllers are used to reduce the overshoot time, undershoot time and settling time are taken less time but PID controllers not satisfactory input signal contains noise and unwanted harmonics. Cascaded PD-PI controller gives better transient response with less settling time. It is combination of two controllers which takes single input and produces single output value. Cascaded PD-PI controller reduces the over shoot, under shoot times and settling time. Cascaded PD-PI controller structure shown in figure 2.

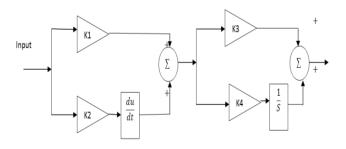


Fig.2 Cascaded controller of PD-PI

# III MODELING OF DFIG WIND TURBINE

In general wind energy does not participate in frequency control. So as to maintain the constant frequency DFIG is added to the AGC. DFIG is used to active power to be controlled required by the system operations. DFIG wind turbine active frequency control shown in figure [3]. Additional control signals are considered  $\Delta P^*f$  is a wind power set point based on the frequency, it produces maximum power.

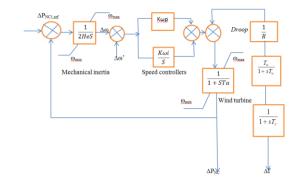


Fig.3 DFIG wind turbine

# IV. HYBRIDIZATION OF PSO AND FA (HPSOFA)

Firefly to another firefly is calculated as shown in Eq.3.

$$r_{ab} = \sqrt{\sum_{k=1}^{d} (x_{a,k} - x_{b,k})^2}$$
 (3)

When ever Light intensity Firefly a is less than the firefly b then a is moved towards b, then update the particle position using Eq.4

$$x_a = x_a + \lceil \beta(r) \rceil (x_b - x_a) + \alpha (rand) \quad (4)$$

Problems in the firefly algorithm overcome with the hybridization of FA with PSO. The velocity equation in PSO is modified by replacing acceleration constants with FAparameters.

$$V_i^{k+1} = wV_i^k + \beta_0 e^{-\gamma r_{ij}^2} \left( Pbest - Z_i \right) + \alpha \left( rand - \frac{1}{2} \right) \left( Gbest - Z_i \right) (5)$$

### V ANALYSIS OF RESULTS

Hybridization algorithm used to tune the gains of PID and cascaded PD-PI controllers by considering the ITAE as objective function. The performance of the considered system is analyzed using PID and PD-PI controllers. Frequency deflection in area 1 without DFIG wind turbine are fig. 4 and frequency deflection in area 2 without DFIG wind turbine are shown in fig. 5. Tie line deviation without DFIG wind turbine shown in fig. 6.

$$ITAE = \int_{0}^{t} (\left| \Delta f_{1} \right| + \left| \Delta f_{2} \right| + \left| \Delta P_{tie} \right|) t. dt$$
 (6)

Two area three units interconnected thermal power system with DFIG wind turbine, both areas connected to the DFIG wind turbine. Three levels of wind penetration i.e. 5%, 20% and 50% are taken into the consideration. It is observed that the lower wind penetration levels shows less settling time and improves the performance. Three levels of wind penetrations applied for the both controllers i.e. PID and cascaded PD-PI controllers. Deviation in area 1 with DFIG wind turbine shown in fig.7 and area2 fig.8 and tie line fig.9 for PID controllers. Cascaded PD-PI controller frequency deviation in area1 with wind turbine shown in fig. 10, and area2 shown in fig.11, and tie line power shown in fig.13. The wind penetration values are shown in table4 [9].





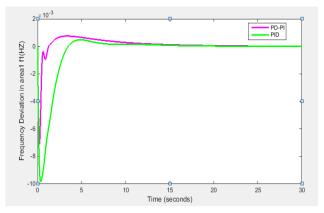


Fig 4.Frequency deviation in area1 without DFIG

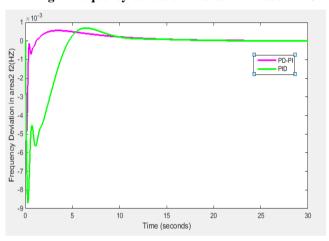


Fig.5.Frequency deviation in area2 without DFIG

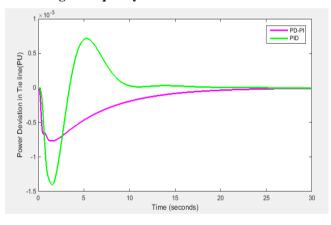


Fig.6. Tieline power deviation without DFIG

 $\begin{array}{l} TABLE\ 1\ . Peak\ overshoots\ (O_{sh}),\ Peak\ undershoots\ (U_{sh}),\ Settling\ time\ (T_s)\ of\ different\ controllers \end{array}$ 

Controllers		Area1( $\Delta f_1$ )	Area2( $\Delta f_2$ )	$\begin{array}{c} \text{Tie} \\ \text{line}(\Delta P_{tie}) \end{array}$
	$U_{sh}$	-0.0098	-0.0086	-0.0014
	$O_{\mathrm{sh}}$	0.0004	0.0007	0.00071
PID	$T_{\rm s}$	9.32	9.6	13.25
	$U_{\rm sh}$	-0.0071	-0.0049	-0.00076
	$O_{\mathrm{sh}}$	0.0003	0.0005	0.0001
PD-PI	$T_{\rm s}$	2.48	2.68	19.03

# A.Frequency deviation with DFIG wind turbine with PID controller.

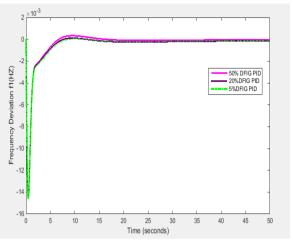


Fig..7 frequency in area 1 with DFIG wind turbine

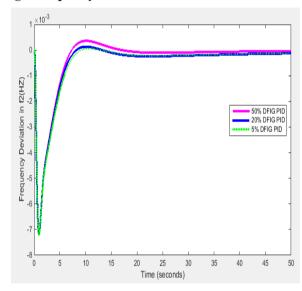


Fig.8 Frequency deviation in area 2 with DFIG wind turbine

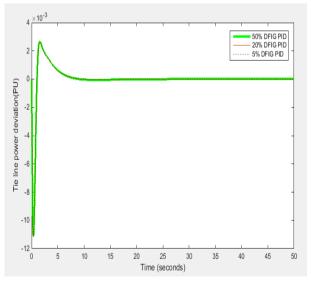


Fig. 9 Tie line power deviation with DFIG wind turbine



TABLE 2. Peak undershoots  $(U_{sh})$ , Peak over shoot  $(O_{sh})$ , and Settling time  $(T_s)$ .

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Percentage		$\Delta f_1$	$\Delta f_2$	$\Delta P_{\text{tie line}}$
	$\mathrm{U}_{\mathrm{sh}}$	-0.01444	-0.0078	-0.011
5%	$O_{\mathrm{sh}}$	0.0005	0.00066	0.00026
	$T_{sh}$	8.68	9.3	8.89
	$U_{\rm sh}$	-0.0017	-0.00719	-0.0110
20%	$O_{sh}$	0.0145	0.00013	0.0025
	$T_s$	9.5	9.85	9.95
	$U_{sh}$	-0.0146	-0.0072	-0.0112
50%	$O_{sh}$	0.003325	0.0036	0.00268
	$T_s$	14.04	14.55	18.55

B.Frequency deviation with DFIG wind turbine with cascaded PD-PI controller.

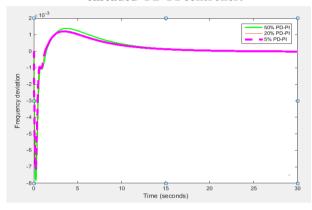


Fig.10 Frequency deviation in area1 with DFIG wind turbine

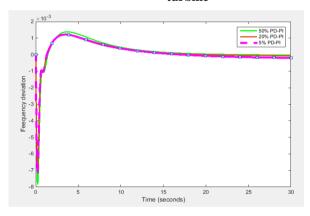


Fig.11Frequency deviation in area2 with DFIG wind turbine.

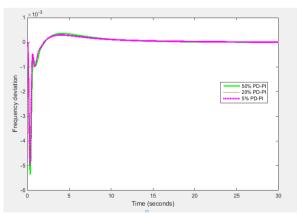


Fig.11Tie line power deviation with DFIG wind turbine.

TABLE 3. Under shoot  $(U_{sh})$ , Peak over shoot  $(O_{sh})$ , and Settling time  $(T_s)$ . For cascaded PD-PI controller

Percentage		$\Delta f_1$	$\Delta f_2$	$\Delta P_{\text{tie line}}$
5%	U sh	-0.0070	-0.0040	-0.00496
	O sh	0.00012	0.00092	0.000296
	T s	9.7	9.4	11.4
20%	U sh	-0.0074	-0.0055	-0.00119
	O sh	0.0012	0.00094	0.00035
	T s	9.8	9.5	11.54
50%	U sh	-0.0073	-0.004	-0.114
	O sh	0.0014	0.00010	0.00036
	T s	10	9.9	11.6
	E 4 0 41			11 0

TABLE 4.Optimum values of speed controller for different DFIG wind turbine penetrations levels

Wind penetration	$K_{\omega p1}$	$K_{\omega i1}$	$K_{\omega p2}$	$K_{\omega i2}$
5%	1.2	0.1	1	0.1
20%	2	0.3	1.98	0.1
50%	1.7	0.2	0.1	1.0

TABLE 5.Optimum gain values of PID controller tuned by Hybridization algorithm.

PID controller	Area1	Area2
K <sub>p</sub>	3.7689	3.8548
K <sub>i</sub>	2.3458	3.8628
K <sub>d</sub>	1.8773	2.9586

TABLE 6.Optimum gain values of cascaded PD-PI tuned by hybridization algorithm.

tuned by hypridization disprimin:				
PI-PD controller	Area1	Area2		
$K_p$	1.7156	0.5565		
$K_{i}$	1.9989	1.9998		
$K_p$	1.7656	1.9669		
$K_{\mathrm{d}}$	1.9877	0.5586		

# VI CONCLUSION

The dynamic performance of AGC has been carried out for two-area multi-unit interconnected power system with DFIG, Area1 consists of three reheat turbines and area2 consists of three non-reheat turbine units and both areas interconnected to DFIG wind turbine. 1% step load disturbance is applied in area 1 to study the dynamic performance. Hybridization optimization technique is used for tuning of both controllers. It is observed that Cascaded PD-PI controller is better than PID controller in all aspects. The frequency response is improved by using DFIG wind turbine. The performance of the PID controller and PD-PI controller is also studied for different penetration levels. It is also observed that Lower penetration gives the best performance as compared to higher penetration levels





APPENDIX I
For thermal power system

For thermal power system			
Parameter	Symbol	Value	
Frequency bias factor	В	0.4249	
Governor time constant	$T_{\mathrm{G}}$	0.08	
Turbine time constant	$T_{\mathrm{T}}$	0.3	
Re heat time constant	T <sub>R</sub>	10	
Control area gain	K <sub>P</sub>	120	
Regulation	R	2.4	
Synchronization time constant	T	0.0866	
Re heat gain	K <sub>R</sub>	0.5	
Area participation factors	APF	0.33	
Control area time constant	$T_p$	20	

### **DFIG** wind turbine parameters

Parameter	Area1	Area2	Value
Wind turbine inertia	$H_{e1}$	$H_{e2}$	3.5
DFIG proportional controller gain	$K_{\omega p1}$	$K_{\omega p2}$	1
DFIG turbine	$T_{a1}$	T <sub>a2</sub>	0.2
Transducer time constant	$T_{r1}$	$T_{r2}$	15
Wash out filter time constant	$T_{\omega 1}$	$T_{\omega 2}$	6
Regulation	$R_1$	$R_2$	2.4

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